## 30 V Input 3 A Buck DC/DC Converter

NO.EA-191-170607

## OUTLINE

The R1242S is a CMOS-based 30 V input, 3 A , synchronous rectified step-down DC/DC converter with builtin High-side switch. The R1242S contains Nch High-side Tr. (Typ. $0.1 \Omega$ ) and can supply maximum 3 A output current. In order to reduce heat generation caused by energy loss, FET can be used as Low-side switch. Lowside switch turns off when ICs shut down. The R1242S consists of the followings: an oscillator, a PWM control circuit, a voltage reference unit, an error amplifier, a phase compensation circuit, a slope control circuit, a softstart circuit, protection circuits, an internal regulator, a switch, and so on. Also, the R1242S consists of the following external components: an inductor, resistors, an external FET, and capacitors.
The R1242S operates with current mode topology, which does not require any sense resistor. As a result, the R1242S can achieve high speed and high efficiency. The oscillator frequencies for each version are set as follows; adjustable between 330 kHz to 1000 kHz for versions $A$ and $B, 330 \mathrm{kHz}$ for versions C and $\mathrm{D}, 500 \mathrm{kHz}$ for versions E and F, and 1000 kHz for versions G and H .
The R1242S is equipped with the protection functions, such as peak current limit function, latch function, fold back function, thermal-shutdown function, and undervoltage-lockout (UVLO) function. Peak current limit function restricts the maximum current into 4.5 A . Latch function (comes with versions $\mathrm{A}, \mathrm{C}, \mathrm{E}$, and G ) shuts off the output if current limit detection continues for a certain period of time. Fold back function (comes with versions $B, D, F$, and $H$ ) reduces the initial oscillator frequencies into $1 / 4$ when output is short-circuited.

## FEATURES

- Supply Current.

Typ. $0.8 \mathrm{~mA}\left(\mathrm{~V}_{\mathrm{IN}}=30 \mathrm{~V}\right.$, Set $\left.\mathrm{V}_{\mathrm{FB}}=1.0 \mathrm{~V}\right)$

- Standby Current

Typ. $0 \mu \mathrm{~A}\left(\mathrm{~V}_{\mathrm{IN}}=30 \mathrm{~V}, \mathrm{CE}=\mathrm{L}\right)$

- Input Voltage Range 5 V to 30 V
- Output Voltage Range 0.8 V to 15 V , Adjustable using external resistors
- Feed Back Voltage Accuracy 0.8 V with $1.5 \%$ accuracy
- Output Current . 3 A
- Oscillator Frequency........................................................ 330 kHz to 1 MHz (Ver. A/B), 330 kHz (Ver. C/D), 500 kHz, (Ver. E/F), 1000 kHz (Ver. G/H)
- Maximum Duty Cycle. Typ. 88\%
- UVLO Detector Threshold .................................................Typ. 3.6 V
- Soft-start Time ................................................................. Typ. 0.5 ms
- Peak Current Limit .Typ. 4.5 A
- Thermal Shutdown Typ. $160^{\circ} \mathrm{C}$
- Latch Type Protection Delay Time: Typ. 5 ms (Ver. A/C/E/G)
- Fold-back Type Protection Fold-back Frequency: Ver. B: fosc x $1 / 4$, Ver. D: 83 kHz, Ver. F: 125 kHz, Ver. H: 250 kHz
- Package HSOP-8E
* This is an approximate value. The output current depends on conditions and external parts.

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## APPLICATIONS

- Digital Home Appliances: Digital TVs, DVD Players
- Office Automation Equipment: Printers, Fax
- Hand-held Communication Equipment: Cameras, Video Recorders
- Battery-powered Equipment


## SELECTION GUIDE

The oscillator frequency (Adjustable, Fixed: 330 kHz, $500 \mathrm{kHz}, 1000 \mathrm{kHz}$ ) and the short-circuit protection type (Latch, Fold-back) are user-selectable options.

## Selection Guide

| Product Name | Package | Quantity per Reel | Pb Free | Halogen Free |
| :---: | :---: | :---: | :---: | :---: |
| R1242S001*-E2-FE | HSOP-8E | 1,000 pcs | Yes | Yes |

* : Specify the oscillator frequency and the short-circuit protection type.

| Code | Frequency | Latch Type | Fold-back Type |
| :---: | :---: | :---: | :---: |
| A | Adjustable | Yes | No |
| B | Adjustable | No | Yes |
| C | 330 kHz | Yes | No |
| D | 330 kHz | No | Yes |
| E | 500 kHz | Yes | No |
| F | 500 kHz | No | Yes |
| G | 1000 kHz | Yes | No |
| H | 1000 kHz | No | Yes |

## BLOCK DIAGRAM


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| Version | Oscillator Frequency | Short Protection |
| :---: | :---: | :---: |
| A | Adjustable | Latch Type |
| B | Adjustable | Fold-back Type |
| C | 330 kHz | Latch Type |
| D | 330 kHz | Fold-back Type |
| E | 500 kHz | Latch Type |
| F | 500 kHz | Fold-back Type |
| G | 1000 kHz | Latch Type |
| H | 1000 kHz | Fold-back Type |

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## PIN DESCRIPTIONS

Top View


HSOP-8E Pin Configuration

## R1242S001A/B Pin Description

| Pin No. | Symbol | Description |
| :---: | :---: | :--- |
| 1 | CE | Chip Enable Pin, Active with "H" |
| 2 | EXT | Gete Drive Pin |
| 3 | BST | Bootstrap Pin |
| 4 | VIN | Power Supply Pin |
| 5 | Lx | Lx Switching Pin |
| 6 | GND | Ground Pin |
| 7 | VFB | Feedback Pin |
| 8 | RT | Frequency Setting Pin |

* Tab is GND level. (They are connected to the reverse side of this IC.) The tab must be connected to the GND.


## R1242S001C/D/E/F/G/H Pin Description

| Pin No. | Symbol | Description |
| :---: | :---: | :--- |
| 1 | CE | Chip Enable Pin, Active with "H" |
| 2 | EXT | Gate Drive Pin |
| 3 | BST | Bootstrap Pin |
| 4 | VIN | Power Supply Pin |
| 5 | Lx | Lx Switching Pin |
| 6 | GND | Ground Pin |
| 7 | VFB | Feedback Pin |
| 8 | TEST | TEST Pin, OPEN or connect to GND |

* Tab is GND level. (They are connected to the reverse side of this IC.) The tab must be connected to the GND.


## ABSOLUTE MAXIMUM RATINGS



* Refer to Power Dissipation for detailed information.


## ABSOLUTE MAXIMUM RATINGS

Electronic and mechanical stress momentarily exceeded absolute maximum ratings may cause the permanent damages and may degrade the life time and safety for both device and system using the device in the field.
The functional operation at or over these absolute maximum ratings is not assured.

## RECOMMENDED OPERATING CONDITIONS

Recommended Operating Conditions

| Symbol | Item | Rating | Unit |
| :---: | :--- | :---: | :---: |
| $\mathrm{V}_{\text {IN }}$ | Operating Input Voltage | 5 to 30 | V |
| Ta | Operating Temperature Range | -40 to 85 | ${ }^{\circ} \mathrm{C}$ |

## RECOMMENDED OPERATING CONDITIONS

All of electronic equipment should be designed that the mounted semiconductor devices operate within the recommended operating conditions. The semiconductor devices cannot operate normally over the recommended operating conditions, even if when they are used over such conditions by momentary electronic noise or surge. And the semiconductor devices may receive serious damage when they continue to operate over the recommended operating conditions.

## ELECTRICAL CHARACTERISTICS

Electrical Characteristics
(Unless otherwise noted, $\mathrm{V}_{\mathrm{IN}}=12 \mathrm{~V}, \mathrm{Ta}=25^{\circ} \mathrm{C}$ )

| Symbol | Item | Conditions | Min. | Typ. | Max. | Unit |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| In | VIN Consumption Current | $\mathrm{V}_{\text {IN }}=30 \mathrm{~V}, \mathrm{~V}_{\mathrm{FB}}=1.0 \mathrm{~V}$ | 0.45 | 0.80 | 1.20 | mA |
| Vuvlo2 | UVLO Detect Voltage | Rising | $\begin{gathered} \hline \text { VUVLO2 } \\ -0.5 \end{gathered}$ |  | $\begin{gathered} \hline \text { VUVLO2 } \\ -0.3 \end{gathered}$ | V |
| Vuvlo1 | UVLO Released Voltage | Falling | 3.7 | 4.0 | 4.3 | V |
| $\mathrm{V}_{\text {FB }}$ | VFB Voltage Tolerance |  | 0.788 | 0.800 | 0.812 | V |
| $\Delta \mathrm{V}_{\mathrm{FB}} / \Delta \mathrm{Ta}$ | VFB Voltage Temperature Coefficient | $-40^{\circ} \mathrm{C} \leq \mathrm{Ta} \leq 85^{\circ} \mathrm{C}$ |  | $\pm 100$ |  | ppm/ ${ }^{\circ} \mathrm{C}$ |
| fosc | Oscillator Frequency (Ver. A/B) | RT = GND | 900 | 1000 | 1100 | kHz |
|  |  | RT = floating | 290 | 330 | 375 | kHz |
|  |  | $\mathrm{RT}=120 \mathrm{k} \Omega$ | 450 | 500 | 550 | kHz |
|  | Oscillator Frequency (Ver. C/D) |  | 300 | 330 | 370 | kHz |
|  | Oscillator Frequency (Ver. E/F) |  | 450 | 500 | 550 | kHz |
|  | Oscillator Frequency (Ver. G/H) |  | 900 | 1000 | 1100 | kHz |
| ffLb | Fold back Frequency | $\begin{aligned} & \hline \mathrm{V}_{\mathrm{FB}}<0.56, \\ & \mathrm{RT}=\mathrm{GND}(\text { Ver. } \mathrm{B}) \\ & \hline \end{aligned}$ |  | 250 |  | kHz |
|  |  | $\mathrm{V}_{\mathrm{FB}}<0.56$ (Ver. D) |  | 83 |  | kHz |
|  |  | $\mathrm{V}_{\text {FB }}<0.56$ (Ver. F) |  | 125 |  | kHz |
|  |  | $\mathrm{V}_{\text {FB }}<0.56$ (Ver. H) |  | 250 |  | kHz |
| Maxduty | Maximum Duty Cycle | $\begin{aligned} & \mathrm{RT}=120 \mathrm{k} \Omega(\text { Ver. } \mathrm{A} / \mathrm{B}) \\ & \mathrm{VIN}=9 \mathrm{~V}(\text { Ver. C/D) } \end{aligned}$ | 82 | 88 | 95 | \% |
| tstart | Soft Start Time |  |  | 0.5 |  | ms |
| tDLY | Delay Time for Latch Protection | (Ver. A/C/E/G) |  | 5 |  | ms |
| RLXH | Lx High Side Switch ON Resistance |  |  | 0.1 |  | $\Omega$ |
| ILXHOFF | Lx High Side Switch Leakage Current |  |  | 0 | 20 | $\mu \mathrm{A}$ |
| ILImLxH | Lx High Side Switch Limited Current |  |  | 4.5 |  | A |
| $V_{\text {ceh }}$ | CE "H" Input Voltage |  | 1.7 |  |  | V |
| Vcel | CE "L" Input Voltage |  |  |  | 0.4 | V |
| IfB | VFB Input Current |  | -1.0 |  | 1.0 | $\mu \mathrm{A}$ |
| Icen | CE "H" Input Current |  | -1.0 |  | 1.0 | $\mu \mathrm{A}$ |
| Icel | CE "L" Input Current |  | -1.0 |  | 1.0 | $\mu \mathrm{A}$ |
| Ttsd | Thermal Shutdown Detect Temperature | Hysteresis: $30^{\circ} \mathrm{C}$ |  | 160 |  | ${ }^{\circ} \mathrm{C}$ |
| Istandby | Standby Current | $\mathrm{V}_{\text {IN }}=30 \mathrm{~V}, \mathrm{~V}_{\text {ce }}=0 \mathrm{~V}$ |  | 0 | 20 | $\mu \mathrm{A}$ |
| RRISE | EXT "H" Switch On Resistance | $\mathrm{IEXT}^{\text {e }}=-100 \mathrm{~mA}$ | 6 |  | 11 | $\Omega$ |
| RFALL | EXT "L" Switch On Resistance | $\mathrm{IEXT}=100 \mathrm{~mA}$ | 0.5 |  | 1.5 | $\Omega$ |
| $\mathrm{V}_{\text {extlim }}$ | Detecting Voltage for Low Side Switch Current Limit |  | 36 | 55 | 76 | mV |

## OPERATING DESCRIPTIONS

## OPERATION OF STEP-DOWN DCIDC CONVERTER AND OUTPUT CURRENT

The step-down DC/DC converter charges energy in the inductor ( L ) when the Lx transistor turns on, and discharges the energy from the inductor when Lx transistor turns off and controls with less energy loss, so that a lower output voltage ( $\mathrm{V}_{\text {out }}$ ) than the input voltage ( $\mathrm{V}_{\mathrm{II}}$ ) can be obtained. The operation of the step-down DC/DC converter is explained in the following figures.


Basic Circuit


Inductor Current flowing through Inductor

Step1. The highside transistor turns on and the inductor current (i1) flows, $L$ is charged with energy. At this moment, i1 increases from the minimum inductor current (ILmin), which is 0 A , and reaches the maximum inductor current (ILmax) in proportion to the on-time period (ton) of the highside transistor.
Step2. When the highside transistor turns off, $L$ tries to maintain IL at ILmax, so $L$ turns the lowside FET on and the inductor current (i2) flows into L.
Step3. i2 decreases gradually and reaches ILmin in proportion to the off-time period (toff) of the highside transistor.

In the case of PWM mode, Vout is maintained by controlling ton. During PWM mode, the oscillator frequency (fosc) is being maintained constant.

When the step-down DC/DC operation is constant, ILmin and ILmax during ton of highside transistor would be same as during toff of highside transistor.

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## APPLICATION INFORMATION

## TYPICAL APPLICATION CIRCUIT



R1242S001A/B Typical Application Circuit, Vout $=1.8$ V, 330 kHz


R1242S001C/D Typical Application Circuit, Vout $=1.2 \mathrm{~V}, 330 \mathrm{kHz}$

## Recommendation Parts

| C $_{\text {IN }}$ | $10 \mu \mathrm{~F}$, KTS500B106M55N0T00 (Nippon Chemi-Con) |
| :---: | :--- |
| Cout $^{\text {Cbst }}$ | $22 \mu \mathrm{~F}$, GRM31CR71A226M (Murata) |
| L | $0.1 \mu \mathrm{~F}$, GRM21BB11H104KA01L (Murata) |
| FET | $4.7 \mu \mathrm{H}$, VLF10045T-4R7N6R1 (TDK) |



R1242S001A/B Typical Application Circuit, Vout $=1.2 \mathrm{~V}, 500 \mathrm{kHz}$


R1242S001E/F Typical Application Circuit, Vout $=1.2 \mathrm{~V}, 500 \mathrm{kHz}$

## Recommendation Parts

| $\mathrm{C}_{\mathrm{IN}}$ | $10 \mu \mathrm{~F}$, KTS500B106M55N0T00 (Nippon Chemi-Con) |
| :---: | :--- |
| Cout | $22 \mu \mathrm{~F}$, GRM31CR71A226M (Murata) |
| Cbst | $0.1 \mu \mathrm{~F}$, GRM21BB11H104KA01L (Murata) |
| L | $2.2 \mu \mathrm{H}$, RLF7030T-2R2M5R4 (TDK) |
| FET | TPN11003NL (TOSHIBA) |

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R1242S001A/B Typical Application Circuit, Vout $=3.3$ V, 1000 kHz


R1242S001G/H Typical Application Circuit, Vout $=3.3$ V, 1000 kHz

Recommendation Parts

| CIN $_{\text {IN }}$ | $10 \mu \mathrm{~F}$, KTS500B106M55N0T00 (Nippon Chemi-Con) |
| :---: | :--- |
| Cout $^{\text {Cbst }}$ | $10 \mu \mathrm{~F}$, GRM31CR71E106K (Murata) |
| L | $0.1 \mu \mathrm{~F}$, GRM21BB11H104KA01L (Murata) |
| FET | $4.7 \mu \mathrm{H}$, VLF10045T-4R7N6R1 (TDK) |

## THE VOLTAGE BETWEEN THE BST PIN AND Lx PIN

In the application of the "Bootstrap" Start switching regulator, the R1242S, when the Lx pin voltage becomes equal or less than the BST voltage supply regulator, the BST voltage supply regulator charges the capacitor, Cbst. By this function, even if the Lx pin becomes "H", the high side switch composed of an Nch transistor can be turned on.

Under the condition of PWM operation, the BST voltage supply regulator of the R1242S, while the Lx pin voltage is "L", the voltage between BST pin and GND pin is controlled and maintained the level as of 5 V , then regardless of the voltage drop by the bootstrap switch, the BST voltage supply regulator can drive a high side switch and the low side external MOSFET.

However, if either the maximum duty cycle limit or the low side switch current limit is detected, sampling of the voltage between BST pin and Lx pin is halted, and the output of the BST voltage supply regulator becomes stacked at 5 V as same as a conventional "Bootstrap" Start switching regulator. Depending on the external FET gate capacitance, excessive voltage drop can be caused by bootstrap switching, and also switching failure can be caused by insufficient electrical charge on Cbst. As a result, the desired voltage may not be obtained. Higher frequency requires higher electrical charge. Special attention is required in case of using the device at 1000 kHz.

Events that may trigger such trouble are
(A) Detect of the current limit of low side switch at light load
(B) $\mathrm{V}_{\text {out }}>\mathrm{V}_{\mathrm{IN}} / 2$ and starting the circuit without using CE pin individually or CE pin and VIN are tied and controlled at the same time.
(C) The voltage difference between the input and the output is small and usage at maximum duty cycle is expected.

The countermeasure to avoid the trouble caused by the events above is to use an external diode, Dbst shown in the figure below. The Dbst will charge $\mathrm{C}_{\text {BSt }}$ and prevents the abnormal switching. The supply voltage to Dbst should be in the range from 4.5 V to 6.0 V and if the set output voltage of the R 1242 S is in the range from 4.5 V to 6.0 V , then the output voltage can be used directly as the supply voltage of Dbst. The voltage rating of the diode, Dbst must be $\mathrm{VI}_{\mathrm{N}}$ or more, the forward current of Dbst must be 20 mA or more. Other specifications of the Dbst are not important.


Application Circuit Example

If the auxiliary power source for BST 4.5 V to 6.0 V does not have a bypass capacitor, set $0.1 \mu \mathrm{~F}$ or higher bypass capacitor between the auxiliary power source and GND.

## OPERATING FREQUENCY (VERSION A/B)

In the application circuit of the R1242S001A/B, the 330 kHz operation is selected by leaving Rt open. Connecting a $200 \mathrm{k} \Omega$ to $0 \Omega$ resistor between Rt (pin 8) and ground can be used to set the switching frequency to approximately 450 kHz to 1000 kHz . To calculate the Rt resistor, use the equation below:
*(Between 330 kHz and 450 kHz switching frequency can be also set by connecting the appropriate resistor according to the next equation.)
$R \mathrm{Rt}=120000 /(2 /(1000000 /$ fosc -1$)-1)[\Omega]$
The switching frequency vs. Rt value is shown in Figure 1 and Figure 2.


Figure 1. Linearscale


Figure 2. Logscale

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## OUTPUT CURRENT AND SELECTION OF EXTERNAL COMPONENTS

The following equations explain the relationship between output current and peripheral components.

Ripple Current P-P value is described as IRP, ON resistance of Highside Tr. is described as Ronh, ON resistance of Lowside FET is described as Ronl, and DC resistance of the inductor is described as RL.

First, when Highside Tr. is "ON", the following equation is satisfied.
$\mathrm{V}_{\text {IN }}=\mathrm{V}_{\text {OUT }}+\left(\right.$ RONH $\left.+\mathrm{R}_{\mathrm{L}}\right) \times$ lout $+\mathrm{L} \times \mathrm{I}_{\text {RP }} /$ ton $\qquad$ Equation 3

Second, when Highside Tr. is "OFF" (Lowside FET is "ON"), the following equation is satisfied.
$L \times I_{R P} /$ toff $=$ RonL $\times$ lout $+V_{\text {OUT }}+$ RL $\times$ lout
Equation 4

Put Equation 4 into Equation 3 to solve ON duty of Highside Tr. (Don $=$ ton / (toff + ton)):
$\mathrm{D}_{\text {ON }}=\left(\mathrm{V}_{\text {OUT }}+\left(\mathrm{R}_{\text {ONL }}+\mathrm{R}_{\mathrm{L}}\right) \times\right.$ loUt $) /\left(\mathrm{V}_{\text {IN }}+\left(\mathrm{R}_{\text {ONL }}-\mathrm{R}_{\text {ONH }}\right) \times\right.$ IOUT $)$
Equation 5

Ripple Current is described as follows:
$I_{R P}=\left(\mathrm{V}_{\text {IN }}-\right.$ V OUt - RoNH $\times$ lout $-\mathrm{R}_{\mathrm{L}} \times$ lout $) \times$ Don $/$ fosc $/ L$ $\qquad$ Equation 6

Peak current that flows through $L$, and $L x$ Tr. is described as follows:
$\mathrm{ILmax}=\mathrm{l}_{\mathrm{lout}}+\mathrm{I}_{\mathrm{RP}} / 2$
Equation 7

Notes: Please consider ILmax when setting conditions of input and output, as well as selecting the external components. The above calculation formulas are based on the ideal operation of the ICs in continuous mode.

## TECHNICAL NOTES

The performance of a power source circuit using this device is highly dependent on a peripheral circuit. A peripheral component or the device mounted on PCB should not exceed its voltage, current or power ratings. When designing a peripheral circuit, please be fully aware of the following points. (Refer to our PCB layout for detailed information).

- External components must be connected as close as possible to the ICs and their wiring must be short as possible. Especially, the capacitor must be connected with the shortest distance between $\mathrm{V}_{\mathbb{I}}$ and GND pins. If the impedances of the power supply line and the GND line are high, the operation can be unstable due to the switching current which fluctuates the electric potential of the inside the ICs. The impedances of power supply line and GND line must be as low as possible. When designing their wirings, it is necessary to give careful consideration to the large current flowing into the power supply, GND, Lx, VOUT and inductor. The wiring of output voltage setting resistance (R1) and the wiring of inductor must be separated from load wiring.
- The ceramic capacitors with low ESR (Equivalent Series Resistance) must be used for the ICs. The recommended value for the $\mathrm{C}_{\mathrm{IN}}$ capacitor between VIN and GND is equal or more than $10 \mu \mathrm{~F}$.
- The selections of inductor (L) and output capacitor (Cout) can be different according to the ICs' oscillation frequencies, output voltages and input voltages. Refer to "Recommended Value for Each Output Voltage" on the next page and select the most suitable values at the conditions of use. The internal phase compensation is built in the ICs; therefore, if the values selected are largely deviated from the recommended values, the operation may result in unstable.
- The over current protection circuit could be influenced by self-heating of the ICs and heat dissipation of the PCB environment.
- In order to prevent self-turning on, FET with smaller gate resistance and with smaller Cgd/ Cgs (capacities between gate drains and the capacities between gate sources) should be selected.
- The output voltage (Vоut) can be calculated as $\mathrm{V}_{\text {out }}=\mathrm{V}_{\mathrm{FB}} \times(\mathrm{R} 1+\mathrm{R} 2) / \mathrm{R} 2$. The various voltage settings are possible by changing the values of R1 and R2. However, R2 value must be equal or less than $16 \mathrm{k} \Omega$.
- Rspd prevents the deterioration in the regulation characteristics, which is caused by spike noise occurred in Vout. Spike noise is largely depending on the PCB layout. If the PCB board layout is optimized, there is no need of Rspd; however, if the spike noise is a concern, Rspd with $15 \Omega$ or so should be used.
- After the completion of soft start, latch function (Ver. A, C, E, G) starts to work. The internal counter starts counting up when the over current protection circuit activates the limited current detection. When the internal counter counts up to 5 ms , which is a typical delay time for latch protection, the latch function turns off the output. The turned off output can be reset when CE pin is changed to "L", and also VIN pin voltage is became less than 3.6 V (Typ.), which is UVLO detecting voltage. If the output voltage increases more than the setting voltage (VFB pin voltage is 0.8 V (Typ.)) within the delay time for latch protection, the counter restores the default. If the power-supply voltage's start-up is slow and the output voltage is not reached to the setting voltage within the delay time for latch protection after the soft start, the careful attention is required.


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- After the soft start, fold back function (Ver. B, D, F, H) starts to work. The fold back function limits the oscillation frequencies into $1 / 4$ when (VFB pin voltage decreases to less than 0.56 V (Typ.)). If the powersupply voltage's start-up is slow and the output voltage is not reached to the $70 \%$ of the setting voltage even for a short period of time after the soft start, the careful attention is required.
- The ICs are not supporting Nonsynchronous rectification using a diode as a rectifier.

The following table shows the recommended values for setting frequency and setting output voltage.

## Recommended Values

330 kHz

| $\mathrm{V}_{\text {OUt }}[\mathrm{V}]$ | 0.8 | 1.2 | 1.2 | 1.5 | 1.5 | 1.8 | 1.8 | 2.5 | 2.5 | 3.3 | 5 | 9 | 15 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{~V}_{\text {IN }}$ Range $[\mathrm{V}]$ | $5 \sim 14$ | $\sim 12$ | $9 \sim 30$ | $5 \sim 10$ | $10 \sim 30$ | $5 \sim 15$ | $12 \sim 30$ | $5 \sim 15$ | $12 \sim 30$ | $5 \sim 30$ | $7 \sim 30$ | $15 \sim 30$ | $20 \sim 30$ |
| $\mathrm{~L}[\mu \mathrm{H}]$ | 2.2 | 10 | 4.7 | 10 | 4.7 | 15 | 4.7 | 15 | 10 | 15 | 15 | 15 | 15 |
| $\mathrm{C}_{\text {out }[\mu \mathrm{F}]}$ | 100 | 22 | 44 | 22 | 44 | 22 | 44 | 22 | 22 | 22 | 22 | 22 | 22 |
| Cspd $[\mathrm{pF}]$ | - | 470 | 470 | 220 | 220 | 470 | 220 | 220 | 220 | 220 | 220 | 220 | $220->100$ |
| R1 $[\Omega]$ | - | 8000 | 8000 | 14000 | 14000 | 20000 | 20000 | 34000 | 34000 | 50000 | 84000 | 164000 | 284000 |
| R2 $[\Omega]$ | - | 16000 | 16000 | 16000 | 16000 | 16000 | 16000 | 16000 | 16000 | 16000 | 16000 | 16000 | 16000 |

500 kHz

| $\mathrm{V}_{\text {Out }}[\mathrm{V}]$ | 0.8 | 1.0 | 1.2 | 1.5 | 1.5 | 1.8 | 1.8 | 2.5 | 3.3 | 5 | 9 | 12 | 15 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{V}_{\text {IN }}$ Range [V] | $\sim 9$ | $\sim 10$ | 5~15 | 5~18 | 7~19 | 5~23 | 9~21 | 5~29 | 5~30 | 7~30 | 15~30 | 18~30 | 20~30 |
| $\mathrm{L}[\mu \mathrm{H}]$ | 2.2 | 2.2 | 2.2 | 4.7 | 2.2 | 4.7 | 2.2 | 10 | 10 | 10 | 10 | 15 | 15 |
| $\mathrm{C}_{\text {out }}[\mu \mathrm{F}]$ | 100 | 44 | 44 | 44 | 44 | 44 | 44 | 22 | 22 | 22 | 22 | 22 | 22 |
| Cspd [pF] | - | 1000 | 470 | 220 | 220 | 220 | 220 | 220 | 220 | 220 | 220 | 220 | 220 |
| R1[ $\Omega$ ] | - | 4000 | 8000 | 14000 | 14000 | 20000 | 20000 | 34000 | 50000 | 84000 | 164000 | 224000 | 284000 |
| R2 [ $\Omega$ ] | - | 16000 | 16000 | 16000 | 16000 | 16000 | 16000 | 16000 | 16000 | 16000 | 16000 | 16000 | 16000 |

1000 kHz

| $\mathrm{V}_{\text {Out }}[\mathrm{V}]$ | 0.8 | 1.2 | 1.5 | 1.8 | 2.5 | 3.3 | 5 | 5 | 9 | 15 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{~V}_{\text {IN }}$ Range $[\mathrm{V}]$ | $5 \sim 7$ | $5 \sim 10$ | $5 \sim 15$ | $5 \sim 15$ | $5 \sim 19$ | $5 \sim 30$ | $7 \sim 12$ | $12 \sim 30$ | $15 \sim 30$ | $20 \sim 30$ |
| $\mathrm{~L}[\mu \mathrm{H}]$ | 1.5 | 2.2 | 2.2 | 4.7 | 4.7 | 4.7 | 4.7 | 4.7 | 4.7 | 10 |
| $\mathrm{C}_{\text {out }}[\mu \mathrm{F}]$ | 100 | 22 | 22 | 22 | 22 | 10 | 10 | 10 | 10 | 10 |
| Cspd $[\mathrm{pF}]$ | - | 220 | 100 | 220 | 220 | 100 | 100 | 56 | 56 | 100 |
| R1 $[\Omega]$ | - | 8000 | 14000 | 20000 | 34000 | 50000 | 84000 | 84000 | 164000 | 284000 |
| R2 $[\Omega]$ | - | 16000 | 16000 | 16000 | 16000 | 16000 | 16000 | 16000 | 16000 | 16000 |

Recommended External Components

| Symbol | Condition | Value | Parts Name | MFR |
| :---: | :---: | :---: | :---: | :---: |
| $\mathrm{Cln}_{\text {IN }}$ |  | $10 \mu \mathrm{~F} / 50 \mathrm{~V}$ | UMK325BJ106MM-P | TAIYO YUDEN |
|  |  | $10 \mu \mathrm{~F} / 50 \mathrm{~V}$ | CGA6P3X7S1H106K | TDK |
|  |  | $10 \mu \mathrm{~F} / 50 \mathrm{~V}$ | KTS500B106M55NOT00 | Nippon Chemi-Con |
|  |  | $10 \mu \mathrm{~F} / 10 \mathrm{~V}$ | GRM31CR71A106K | Murata |
| Cout | $\mathrm{V}_{\text {OUT }}>10 \mathrm{~V}$ | $10 \mu \mathrm{~F} / 50 \mathrm{~V}$ | KTS500B106M55N0T00 | Nippon Chemi-Con |
|  | $10 \mathrm{~V}>\mathrm{V}_{\text {Out }}>1.8 \mathrm{~V}$ | $10 \mu \mathrm{~F} / 25 \mathrm{~V}$ | GRM31CR71E106K | Murata |
|  | $\mathrm{V}_{\text {OUT }}<1.8 \mathrm{~V}$ | $22 \mu \mathrm{~F} / 10 \mathrm{~V}$ | GRM31CR71A226M | Murata |
|  |  |  | (at the diode rectifier, the specified condition only) |  |
| Cbst |  | $0.1 \mu \mathrm{~F} / 50 \mathrm{~V}$ | GRM21BB11H104KA01L | Murata |
| L | $1.5 \mu \mathrm{H} \pm 30 \% / 4.0 \mathrm{~A}$ | $1.5 \mu \mathrm{H}$ | SLF7055T-1R5N4R0-3PF | TDK |
|  | $2.2 \mu \mathrm{H} \pm 20 \% / 5.4 \mathrm{~A}$ | $2.2 \mu \mathrm{H}$ | RLF7030T-2R2M5R4 | TDK |
|  | $4.7 \mu \mathrm{H} \pm 30 \% / 6.1 \mathrm{~A}$ | $4.7 \mu \mathrm{H}$ | VLF10045T-4R7N6R1 | TDK |
|  | $10 \mu \mathrm{H} \pm 20 \% 6.2 \mathrm{~A}$ | $10 \mu \mathrm{H}$ | VLF12060T-100M6R2 | TDK |
|  | $15 \mu \mathrm{H} \pm 20 \% 5.0 \mathrm{~A}$ | $15 \mu \mathrm{H}$ | VLF12060T-150M5R0 | TDK |
| FET | $30 \mathrm{~V} / 11 \mathrm{~A}$ | $12.6 \mathrm{~m} \Omega$ | TPN11003NL | TOSHIBA |
|  | $30 \mathrm{~V} / 20 \mathrm{~A}$ | $10.2 \mathrm{~m} \Omega$ | TPN8R903NL | TOSHIBA |
|  | $30 \mathrm{~V} / 6 \mathrm{~A}$ | $56 \mathrm{~m} \Omega$ | SSM3K335R | TOSHIBA |
| Rce | The diode is connected between CE pin and VIN pin as an ESD protection element. |  |  |  |
|  | If there is a possibility that the CE pin voltage becomes higher than the VIN pin voltage, |  |  |  |
|  | it is recommended to insert a $5 \mathrm{k} \Omega$ resistance or more in order to prevent the large current |  |  |  |
|  | flowing from CE pin into VIN pin. |  |  |  |

## TECHNICAL NOTES ON PCB LAYOUT PATTERN

1. Make the power line (VIN and GND) broad to avoid the generation of the parasitic inductance. Place the bypass capacitor ( $\mathrm{C}_{\mathrm{IN}}$ ) between VIN and GND as close as possible to each other.
2. Make the wire between Lx pin and the inductor as short as possible to avoid the generation of the parasitic inductance. (This Evaluation Board is designed for the testing. Therefore, the inductor is large, a diode is connectable, and the large space is secured for Lx part.)
3. The ripple current passes through the output capacitor; therefore, if the Cout's GND is placed in the outside of the CIN's GND side and the IC's GND, the IC can be easily affected by the noise.
4. Mount Rup, $\mathrm{R}_{\text {BOt }}, \mathrm{C}_{\text {SPD }}$ and RSPD on the place where the FB pin is close and the inductor and the BST pin are away.
5. Start the feedback from where the output capacitor (Cout) is close.

## PCB LAYOUT

TOP VIEW


BOTTOM VIEW


## TYPICAL CHARACTERISTICS

1)FB Voltage

3)Oscillator Frequency(ver.A,B Rt=GND)

5)Oscillator Frequency(ver.C,D)

2)Oscillator Frequency(ver.A,B Rt=floating)

4)Oscillator Frequency(ver.A,B $R t=120 k \Omega$ )
$\left(\mathrm{V}_{\mathrm{IN}}=12 \mathrm{~V}\right)$

6) Oscillator Frequency(ver.E,F)

$$
\left(\mathrm{V}_{\mathrm{IN}}=12 \mathrm{~V}\right)
$$



## 7) Oscillator Frequency(ver.G,H) <br> 

9) Fold-Back Frequency(ver.C,D)

10) Fold-Back Frequency(ver.G,H)

11) Fold-Back Frequency(ver.A,B Rt=GND)

12) Fold-Back Frequency(ver.E,F)

13) Maxduty(ver.A,B Rt=floating)

14) Maxduty(ver.C,D)


## 15) Maxduty(ver.A,B Rt=GND)


14) Maxduty(ver.G,H)

16) Maxduty(ver.C,D)

17) Maxduty(ver.G,H)


## R1242S

NO.EA-191-170607

## 18)Efficiency vs Load Current fosc $=330 \mathrm{kHz}$ <br> $\mathrm{V}_{\text {out }}: 0.8 \mathrm{~V}$


$\mathrm{V}_{\text {out }}: 15 \mathrm{~V}$


## fosc $=500 \mathrm{kHz}$

V


$$
\mathrm{V}_{\text {out }}: 3.3 \mathrm{~V}
$$



## $\mathrm{V}_{\text {OUT }}: 15 \mathrm{~V}$



$$
\mathrm{V}_{\mathrm{OUT}}: 15 \mathrm{~V}
$$



## R1242S

NO.EA-191-170607

$\mathrm{V}_{\text {out }}: 3.3 \mathrm{~V}$


## $\mathrm{V}_{\text {оит: }}$ :15V



## fosc $=500 \mathrm{kHz}$

$\mathrm{V}_{\text {OUT }}: 0.8 \mathrm{~V}$

$\mathrm{V}_{\text {out }}$ :3.3V


## $\mathrm{V}_{\text {OUT }}: 15 \mathrm{~V}$

V

$\mathrm{V}_{\text {out }}: 15 \mathrm{~V}$


## R1242S

NO.EA-191-170607

$V_{\text {OUT }}: 3.3 \mathrm{~V}$

$\mathrm{V}_{\text {out }}: 15 \mathrm{~V}$


## fosc $=500 \mathrm{kHz}$

$\mathrm{V}_{\text {OUT }}: \mathbf{0 . 8} \mathrm{V}$


## $\mathrm{V}_{\text {OUT }}: 15 \mathrm{~V}$


fosc $=1000 \mathrm{kHz}$
$\mathrm{V}_{\text {OUT }}: 0.8 \mathrm{~V}$

$\mathrm{V}_{\text {out }}: 3.3 \mathrm{~V}$

$\mathrm{V}_{\text {OUT }}: 15 \mathrm{~V}$


The power dissipation of the package is dependent on PCB material, layout, and environmental conditions. The following conditions are used in this measurement.

Measurement Conditions

|  | Ultra-High Wattage Land Pattern |
| :---: | :---: |
| Environment | Mounting on Board (Wind Velocity $=0 \mathrm{~m} / \mathrm{s}$ ) |
| Board Material | Glass Cloth Epoxy Plastic (Four-Layer Board) |
| Board Dimensions | $76.2 \mathrm{~mm} \times 114.3 \mathrm{~mm} \times 0.8 \mathrm{~mm}$ |
| Copper Ratio | Outer Layers (First and Fourth Layers): Approx. $95 \%$ of 50 mm Square <br> Inner Layers (Second and Third Layers): Approx. 100\% of 50 mm Square |
| Through-holes | $\phi 0.4 \mathrm{~mm} \times 21$ pcs |

Measurement Result
$\left(\mathrm{Ta}=25^{\circ} \mathrm{C}, \mathrm{Tjmax}=125^{\circ} \mathrm{C}\right)$

|  | Ultra-High Wattage Land Pattern |
| :---: | :---: |
| Power Dissipation | 2.9 W |
| Thermal Resistance | $\theta \mathrm{ja}=\left(125-25^{\circ} \mathrm{C}\right) / 2.9 \mathrm{~W}=35^{\circ} \mathrm{C} / \mathrm{W}$ |
|  | $\theta \mathrm{jc}=10^{\circ} \mathrm{C} / \mathrm{W}$ |



Power Dissipation vs. Ambient Temperature


Measurement Board Pattern


HSOP-8E Package Dimensions

* The tab on the bottom of the package shown by blue circle is substrate potential (GND). It is recommended that this tab be connected to the ground plane on the board but it is possible to leave the tab floating.

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