## 1:3 LVPECL CLOCK BUFFER + ADDITIONAL LVCMOS OUTPUT AND PROGRAMMABLE DIVIDER

## FEATURES

- Distributes One Differential Clock Input to Three LVPECL Differential Clock Outputs and One LVCMOS Single-Ended Output
- Programmable Output Divider for Two LVPECL Outputs and LVCMOS Output
- Low-Output Skew 15 ps (Typical) for Clock-Distribution Applications for LVPECL Outputs; 1.6-ns Output Skew Between LVCMOS and LVPECL Transitions Minimizing Noise
- $\mathrm{V}_{\mathrm{cc}}$ Range $3 \mathrm{~V}-3.6 \mathrm{~V}$
- Signaling Rate Up to $800-\mathrm{MHz}$ LVPECL and 200-MHz LVCMOS
- Differential Input Stage for Wide Common-Mode Range
- Provides VBB Bias Voltage Output for Single-Ended Input Signals
- Receiver Input Threshold $\pm 75 \mathrm{mV}$
- 24-Terminal QFN Package ( $4 \mathrm{~mm} \times 4 \mathrm{~mm}$ )
- Accepts Any Differential Signaling: LVDS, HSTL, CML, VML, SSTL-2, and Single-Ended: LVTTL/LVCMOS


## DESCRIPTION

The CDCM1804 clock driver distributes one pair of differential clock inputs to three pairs of LVPECL differential clock outputs $\mathrm{Y}[2: 0]$ and $\mathrm{Y}[2: 0]$, with minimum skew for clock distribution. The CDCM1804 is specifically designed for driving $50-\Omega$ transmission lines. Additionally, the CDCM1804 offers a single-ended LVCMOS output Y3. This output is delayed by 1.6 ns over the three LVPECL output stages to minimize noise impact during signal transitions.
The CDCM1804 has three control terminals, S0, S1, and S2, to select different output mode settings. The $\mathrm{S}[2: 0]$ terminals are 3 -level inputs and therefore allow up to $3^{3}=27$ combinations. Additionally, an enable terminal (EN) is provided to disable or enable all outputs simultaneously. The EN terminal is a 3 -level input as well and extends the number of settings to $2 \times 27=54$. See Table - 1 for details.

The CDCM1804 is characterized for operation from $-40^{\circ} \mathrm{C}$ to $85^{\circ} \mathrm{C}$.

For use in single-ended driver applications, the CDCM1804 also provides a VBB output terminal that can be directly connected to the unused input as a common-mode voltage reference.

${ }^{(1)}$ Thermal pad must be connected to $\mathrm{V}_{\mathrm{SS}}$.
P0024-01

RTH PACKAGE
(TOP VIEW)

${ }^{(1)}$ Thermal pad must be connected to $V_{S S}$.

Please be aware that an important notice concerning availability, standard warranty, and use in critical applications of Texas Instruments semiconductor products and disclaimers thereto appears at the end of this data sheet.

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FUNCTIONAL BLOCK DIAGRAM


## TERMINAL FUNCTIONS

| TERMINAL |  | I/O | DESCRIPTION |
| :---: | :---: | :---: | :---: |
| NAME | NO. |  |  |
| EN | 1 | I (with $60-\mathrm{k} \Omega$ pullup) | ENABLE: Enables or disables all outputs simultaneously. The EN terminal offers three different configurations: tied to GND (logic 0 ), external $60-\mathrm{k} \Omega$ pulldown resistor (pull to $\mathrm{V}_{\mathrm{DD}} / 2$ ), or left floating (logic 1); <br> $\mathrm{EN}=1$ : outputs on according to $\mathrm{S}[2: 0]$ settings <br> $\mathrm{EN}=\mathrm{V}_{\mathrm{DD}} / 2$ : outputs on according to $\mathrm{S}[2: 0]$ settings <br> $\mathrm{EN}=0$ : outputs $\mathrm{Y}[3: 0]$ off (high impedance) <br> See Table_1 for details. |
| IN, $\overline{\mathrm{N}}$ | 3, 4 | I (differential) | Differential input clock: Input stage is sensitive and has a wide common-mode range. Therefore, almost any type of differential signal can drive this input (LVPECL, LVDS, CML, HSTL). Because the input is high-impedance, it is recommended to terminate the PCB transmission line before the input (e.g., with $100 \Omega$ across input). Input can also be driven by single-ended signal if the complementary input is tied to VBB. A more-advanced scheme for single-ended signals is given in the Application Information section near the end of this document. <br> The inputs employ an ESD structure protecting the inputs in case of an input voltage exceeding the rails by more than $\sim 0.7 \mathrm{~V}$. Reverse biasing of the IC through these inputs is possible and must be prevented by limiting the input voltage $<\mathrm{V}_{\mathrm{DD}}$. |
| S[2:0] | 18, 19, 24 | (with $60-\mathrm{k} \Omega$ pullup) | Select mode of operation: Defines the output configuration of Y[3:0]. Each terminal offers three different configurations: tied to GND (logic 0), external 60-k $\Omega$ pulldown resistor (pull to $\mathrm{V}_{\mathrm{DD}} / 2$ ), or left floating (logic 1); see Table_1 for details. |
| VBB | 6 | O | Bias voltage output to be used to bias unused complementary input $\overline{\mathbb{N}}$ for single-ended input signals. <br> The output voltage of VBB is $\mathrm{V}_{\mathrm{DD}}-1.3 \mathrm{~V}$. When driving a load, the output current drive is limited to about 1.5 mA . |
| $\mathrm{V}_{\text {SS }}$ | 7 | Supply | Device ground |
| $\mathrm{V}_{\text {DD }} \mathrm{PECL}$ | 2, 5 | Supply | Supply voltage LVPECL input + internal logic |
| $\mathrm{V}_{\mathrm{DD}}[2: 0]$ | $\begin{aligned} & 8,11,14 \\ & 17,20,23 \end{aligned}$ | Supply | LVPECL output supply voltage for output Y[2:0]. Each output can be disabled by pulling the corresponding $\mathrm{V}_{\mathrm{DD}} \mathrm{x}$ to GND. <br> CAUTION: In this mode, no voltage from outside may be forced, because internal diodes could be forced in forward direction. Thus, it is recommended to disconnect the output. |
| $\mathrm{V}_{\mathrm{DD}} 3$ | 13 | Supply | Supply voltage LVCMOS output. The LVCMOS output can be disabled by pulling $\mathrm{V}_{\mathrm{DD}} 3$ to GND. <br> CAUTION: In this mode, no voltage from outside may be forced because internal diodes could be forced in a forward direction. Thus, it is recommended to leave Y3 unconnected, tied to GND, or terminated into GND. |
| $\frac{\mathrm{Y}[2: 0]}{\mathrm{Y}[2: 0]}$ | $\begin{gathered} 9,15,21 \\ 10,16,22 \end{gathered}$ | O (LVPECL) | LVPECL clock outputs. These outputs provide low-skew copies of IN or down-divided copies of clock IN based on selected mode of operation S[2:0]. If an output is unused, the output can simply be left open to save power and minimize noise impact to the remaining outputs. |
| Y3 | 12 | O | LVCMOS clock output. This output provides copy of IN or down-divided copy of clock IN based on selected mode of operation S[2:0]. Also, this output can be disabled when $\mathrm{V}_{\mathrm{DD}} 3$ becomes tied to GND. |

## CONTROL TERMINAL SETTINGS

The CDCM1804 has three control terminals (S0, S1, and S2) and an enable terminal (EN) to select different output mode settings. All four inputs (S0, S1, S2, and EN) are 3-level inputs offering 54 different combinations. In addition, the EN input allows the disabling of all outputs and forcing them into a high-z (or 3-state) output state when pulled to GND.

Each control input incorporates a $60-\mathrm{k} \Omega$ pullup resistor. Thus, it is easy to choose the input setting by designing a resistor pad between the control input and GND. To choose a logic zero, the resistor value must be zero. Setting the input high requires leaving the resistor pad empty (no resistor installed). For setting the input to $\mathrm{V}_{\mathrm{DD}} / 2$, the installed resistor must be a $60-\mathrm{k} \Omega$ pulldown to GND with a $10 \%$ tolerance or better.


Figure 1. Control Terminal Setting for Example

Table 1. Selection Mode Table

|  |  |  |  |  | LVPECL ${ }^{(1)}$ |  |  | LVCMOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MODE | EN | S2 | S1 | S0 | YO | Y1 | Y2 | Y3 |
| 0 | 0 | X | X | X | Off (high-z) |  |  |  |
| 1 | 1 | 0 | 0 | 0 | $\div 1$ | $\div 1$ | $\div 1$ | Off (high-z) |
| 2 | 1 | 0 | 0 | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\div 1$ | Off (high-z) | Off (high-z) | $\div 4$ |
| 3 | 1 | 0 | 0 | 1 | $\div 1$ | $\div 1$ | Off (high-z) | $\div 4$ |
| 4 | 1 | 0 | $\mathrm{V}_{\mathrm{DD}} / 2$ | 0 | $\div 1$ | $\div 2$ | Off (high-z) | $\div 4$ |
| 5 | 1 | 0 | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\div 1$ | $\div 4$ | Off (high-z) | $\div 4$ |
| 6 | 1 | 0 | $\mathrm{V}_{\mathrm{DD}} / 2$ | 1 | $\div 1$ | $\div 8$ | Off (high-z) | $\div 4$ |
| 7 | 1 | 0 | 1 | 0 | $\div 1$ | Off (high-z) | $\div 1$ | $\div 4$ |
| 8 | 1 | 0 | 1 | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\div 1$ | $\div 1$ | $\div 1$ | $\div 4$ |
| 9 | 1 | 0 | 1 | 1 | $\div 1$ | $\div 2$ | $\div 1$ | $\div 4$ |
| 10 | 1 | $\mathrm{V}_{\mathrm{DD}} / 2$ | 0 | 0 | $\div 1$ | $\div 4$ | $\div 1$ | $\div 4$ |
| 11 | 1 | $\mathrm{V}_{\mathrm{DD}} / 2$ | 0 | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\div 1$ | $\div 8$ | $\div 1$ | $\div 4$ |
| 12 | 1 | $\mathrm{V}_{\mathrm{DD}} / 2$ | 0 | 1 | $\div 1$ | Off (high-z) | $\div 2$ | $\div 4$ |
| 13 | 1 | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\mathrm{V}_{\mathrm{DD}} / 2$ | 0 | $\div 1$ | $\div 1$ | $\div 2$ | $\div 4$ |
| 14 | 1 | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\div 1$ | $\div 2$ | $\div 2$ | $\div 4$ |
| 15 | 1 | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\mathrm{V}_{\mathrm{DD}} / 2$ | 1 | $\div 1$ | $\div 4$ | $\div 2$ | $\div 4$ |
| 16 | 1 | $\mathrm{V}_{\mathrm{DD}} / 2$ | 1 | 0 | $\div 1$ | $\div 8$ | $\div 2$ | $\div 4$ |
| 17 | 1 | $\mathrm{V}_{\mathrm{DD}} / 2$ | 1 | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\div 1$ | Off (high-z) | $\div 4$ | $\div 4$ |
| 18 | 1 | $\mathrm{V}_{\mathrm{DD}} / 2$ | 1 | 1 | $\div 1$ | $\div 1$ | $\div 4$ | $\div 4$ |
| 19 | 1 | 1 | 0 | 0 | $\div 1$ | $\div 2$ | $\div 4$ | $\div 4$ |
| 20 | 1 | 1 | 0 | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\div 1$ | $\div 4$ | $\div 4$ | $\div 4$ |
| 21 | 1 | 1 | 0 | 1 | $\div 1$ | $\div 8$ | $\div 4$ | $\div 4$ |
| 22 | 1 | 1 | $\mathrm{V}_{\mathrm{DD}} / 2$ | 0 | $\div 1$ | Off (high-z) | $\div 8$ | $\div 4$ |
| 23 | 1 | 1 | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\div 1$ | $\div 1$ | $\div 8$ | $\div 4$ |
| 24 | 1 | 1 | $\mathrm{V}_{\mathrm{DD}} / 2$ | 1 | $\div 1$ | $\div 2$ | $\div 8$ | $\div 4$ |
| 25 | 1 | 1 | 1 | 0 | $\div 1$ | $\div 4$ | $\div 8$ | $\div 4$ |

(1) The LVPECL outputs are open-emitter stages. Thus, if you leave the unused LVPECL outputs Y0, Y1, or Y2 unconnected, then the current consumption is minimized and noise impact to remaining outputs is neglectable. Also, each output can be individually disabled by connecting the corresponding $\mathrm{V}_{\mathrm{DD}}$ input to GND.

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Table 1. Selection Mode Table (continued)

|  |  |  |  |  | LVPECL ${ }^{(1)}$ |  |  | LVCMOS |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| MODE | EN | S2 | S1 | S0 | Y0 | Y1 | Y2 | Y3 |
| 26 | 1 | 1 | 1 | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\div 1$ | $\div 8$ | $\div 8$ | $\div 4$ |
| 27 | 1 | 1 | 1 | 1 | $\div 1$ | Off (high-z) | $\div 16$ | $\div 4$ |
| 28 | $\mathrm{V}_{\mathrm{DD}} / 2$ | 0 | 0 | 0 | $\div 1$ | $\div 1$ | $\div 16$ | $\div 4$ |
| 29 | $\mathrm{V}_{\mathrm{DD}} / 2$ | 0 | 0 | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\div 1$ | $\div 2$ | $\div 16$ | $\div 4$ |
| 30 | $\mathrm{V}_{\mathrm{DD}} / 2$ | 0 | 0 | 1 | $\div 1$ | $\div 4$ | $\div 16$ | $\div 4$ |
| 31 | $\mathrm{V}_{\mathrm{DD}} / 2$ | 0 | $\mathrm{V}_{\mathrm{DD}} / 2$ | 0 | $\div 1$ | $\div 8$ | $\div 16$ | $\div 4$ |
| 32 | $\mathrm{V}_{\mathrm{DD}} / 2$ | 0 | $\mathrm{V}_{\mathrm{DL}} / 2$ | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\div 1$ | Off (high-z) | Off (high-z) | $\div 1$ |
| 33 | $\mathrm{V}_{\mathrm{DD}} / 2$ | 0 | $\mathrm{V}_{\mathrm{DD}} / 2$ | 1 | $\div 1$ | $\div 1$ | Off (high-z) | $\div 1$ |
| 34 | $\mathrm{V}_{\mathrm{DD}} / 2$ | 0 | 1 | 0 | $\div 1$ | $\div 2$ | Off (high-z) | $\div 1$ |
| 35 | $\mathrm{V}_{\mathrm{DD}} / 2$ | 0 | 1 | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\div 1$ | $\div 1$ | Off (high-z) | $\div 2$ |
| 36 | $\mathrm{V}_{\mathrm{DD}} / 2$ | 0 | 1 | 1 | $\div 1$ | $\div 2$ | Off (high-z) | $\div 2$ |
| 37 | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\mathrm{V}_{\mathrm{DD}} / 2$ | 0 | 0 | $\div 1$ | Off (high-z) | Off (high-z) | $\div 2$ |
| 38 | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\mathrm{V}_{\mathrm{DD}} / 2$ | 0 | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\div 1$ | $\div 1$ | $\div 1$ | $\div 2$ |
| 39 | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\mathrm{V}_{\mathrm{DD}} / 2$ | 0 | 1 | $\div 1$ | $\div 2$ | $\div 8$ | $\div 2$ |
| 40 | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\mathrm{V}_{\mathrm{DD}} / 2$ | 0 | $\div 1$ | $\div 2$ | $\div 8$ | $\div 8$ |
| 41 | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\div 1$ | $\div 4$ | Off (high-z) | $\div 1$ |
| 42 | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\mathrm{V}_{\mathrm{DD}} / 2$ | 1 | $\div 1$ | $\div 8$ | Off (high-z) | $\div 1$ |
| 43 | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\mathrm{V}_{\mathrm{DD}} / 2$ | 1 | 0 | $\div 1$ | $\div 4$ | Off (high-z) | $\div 2$ |
| 44 | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\mathrm{V}_{\mathrm{DD}} / 2$ | 1 | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\div 1$ | $\div 8$ | Off (high-z) | $\div 2$ |
| 45 | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\mathrm{V}_{\mathrm{DD}} / 2$ | 1 | 1 | $\div 1$ | $\div 1$ | $\div 2$ | $\div 2$ |
| 46 | $\mathrm{V}_{\mathrm{DD}} / 2$ | 1 | 0 | 0 | $\div 1$ | Off (high-z) | Off (high-z) | $\div 8$ |
| 47 | $\mathrm{V}_{\mathrm{DD}} / 2$ | 1 | 0 | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\div 1$ | $\div 4$ | Off (high-z) | $\div 8$ |
| 48 | $\mathrm{V}_{\mathrm{DD}} / 2$ | 1 | 0 | 1 | $\div 1$ | $\div 4$ | $\div 8$ | $\div 8$ |
| 49 | $\mathrm{V}_{\mathrm{DD}} / 2$ | 1 | $\mathrm{V}_{\mathrm{DD}} / 2$ | 0 | $\div 1$ | $\div 8$ | Off (high-z) | $\div 8$ |
| 50 | $\mathrm{V}_{\mathrm{DD}} / 2$ | 1 | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\div 1$ | $\div 2$ | $\div 8$ | $\div 16$ |
| Rsv | $\mathrm{V}_{\mathrm{DD}} / 2$ | 1 | $\mathrm{V}_{\mathrm{DD}} / 2$ | 1 | Reserved | Reserved | Reserved | Reserved |
| Rsv | $\mathrm{V}_{\mathrm{DD}} / 2$ | 1 | 1 | 0 | N/A | Low | Low | Low |
| 53 | $\mathrm{V}_{\mathrm{DD}} / 2$ | 1 | 1 | $\mathrm{V}_{\mathrm{DD}} / 2$ | $\div 1$ | $\div 1$ | $\div 1$ | $\div 1$ |
| 54 | $\mathrm{V}_{\mathrm{DD}} / 2$ | 1 | 1 | 1 | $\div 1$ | $\div 1$ | $\div 1$ | $\div 1$ |

## ABSOLUTE MAXIMUM RATINGS

over operating free-air temperature (unless otherwise noted) ${ }^{(1)}$

| $\mathrm{V}_{\mathrm{DD}}$ | Supply voltage | -0.3 V to 3.8 V |
| :--- | :--- | :---: |
| $\mathrm{~V}_{\mathrm{I}}$ | Input voltage | -0.2 V to $\left(\mathrm{V}_{\mathrm{DD}}+0.2 \mathrm{~V}\right)$ |
| $\mathrm{V}_{\mathrm{O}}$ | Output voltage | -0.2 V to $\left(\mathrm{V}_{\mathrm{DD}}+0.2 \mathrm{~V}\right)$ |
|  | Differential short-circuit current, $\mathrm{Yn}, \overline{\mathrm{Yn}}, \mathrm{I} \mathrm{IOSD}$ | Continuous |
|  | Electrostatic discharge (HBM $1.5 \mathrm{k} \Omega, 100 \mathrm{pF}), \mathrm{ESD}$ | $>2000 \mathrm{~V}$ |
|  | Moisture level 24-terminal QFN package (solder reflow temperature of $\left.235^{\circ} \mathrm{C}\right) \mathrm{MSL}$ | 2 |
| $\mathrm{~T}_{\text {stg }}$ | Storage temperature | $-65^{\circ} \mathrm{C}$ to $150^{\circ} \mathrm{C}$ |
| $\mathrm{T}_{J}$ | Maximum junction temperature | $125^{\circ} \mathrm{C}$ |

(1) Stresses beyond those listed under "absolute maximum ratings" may cause permanent damage to the device. These are stress ratings only, and functional operation of the device at these or any other conditions beyond those indicated under "recommended operating conditions" is not implied. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

## RECOMMENDED OPERATING CONDITIONS

|  |  | MIN | TYP | MAX |
| :--- | :--- | :---: | :---: | :---: |
| $\mathrm{V}_{\mathrm{DD}}$ | Uupply voltage | 3 | 3.3 | 3.6 |
| $\mathrm{~T}_{\mathrm{A}}$ | Operating free-air temperature | V |  |  |

## ELECTRICAL CHARACTERISTICS

over recommended operating free-air temperature range (unless otherwise noted)

## LVPECL INPUT IN, $\overline{\text { IN }}$

| PARAMETER |  | TEST CONDITIONS | MIN | TYP | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{f}_{\text {clk }}$ | Input frequency |  | 0 |  | 800 | MHz |
| $\mathrm{V}_{C M}$ | High-level input common mode |  | 1 |  | $\mathrm{V}_{\mathrm{DD}}-0.3$ | V |
| $\mathrm{V}_{\mathrm{IN}}$ | Input voltage swing between IN and $\overline{\mathrm{IN}}{ }^{(1)}$ |  | 500 |  | 1300 | mV |
|  | Input voltage swing between IN and $\overline{\mathbb{N}}{ }^{(2)}$ |  | 150 |  | 1300 |  |
| $\mathrm{I}_{\mathrm{N}}$ | Input current | $\mathrm{V}_{1}=\mathrm{V}_{\mathrm{DD}}$ or 0 V |  |  | $\pm 10$ | $\mu \mathrm{A}$ |
| $\mathrm{R}_{\mathrm{IN}}$ | Input impedance |  | 300 |  |  | $\mathrm{k} \Omega$ |
| $\mathrm{C}_{1}$ | Input capacitance at IN, IN |  |  | 1 |  | pF |

(1) Is required to maintain ac specifications
(2) Is required to maintain device functionality

## LVPECL OUTPUT DRIVER Y[2:0], $\overline{\mathrm{Y}[2: 0]}$

| PARAMETER |  | TEST CONDITIONS | MIN | TYP MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{f}_{\text {clk }}$ | Output frequency, see Figure 4 |  | 0 | 800 | MHz |
| $\mathrm{V}_{\mathrm{OH}}$ | High-level output voltage | Termination with $50 \Omega$ to $\mathrm{V}_{\mathrm{DD}}-2 \mathrm{~V}$ | $V_{D D}-1.18$ | $\mathrm{V}_{\mathrm{DD}}-0.81$ | V |
| $\mathrm{V}_{\text {OL }}$ | Low-level output voltage | Termination with $50 \Omega$ to $\mathrm{V}_{\mathrm{DD}}-2 \mathrm{~V}$ | $\mathrm{V}_{\mathrm{DD}}-1.98$ | $\mathrm{V}_{\mathrm{DD}}-1.55$ | V |
| $\mathrm{V}_{\mathrm{O}}$ | Output voltage swing between Y and $\bar{Y}$, see Eigure 4. | Termination with $50 \Omega$ to $\mathrm{V}_{\mathrm{DD}}-2 \mathrm{~V}$ | 500 |  | mV |
| $\mathrm{l}_{\text {OzL }}$ | Output 3-state current | $\mathrm{V}_{\mathrm{DD}}=3.6 \mathrm{~V}, \mathrm{~V}_{\mathrm{O}}=0 \mathrm{~V}$ |  | 5 | $\mu \mathrm{A}$ |
| $\mathrm{I}_{\mathrm{OzH}}$ |  | $\mathrm{V}_{\mathrm{DD}}=3.6 \mathrm{~V}, \mathrm{~V}_{\mathrm{O}}=\mathrm{V}_{\mathrm{DD}}-0.8 \mathrm{~V}$ |  | 10 |  |
| $\mathrm{t}_{\mathrm{r}} / \mathrm{t}_{\text {f }}$ | Rise and fall time | $20 \%$ to $80 \%$ of $V_{\text {OUTPP }}$, see Eigure 9 | 200 | 350 | ps |
| $\mathrm{t}_{\text {skpecl(0) }}$ | Output skew between any LVPECL output $\mathrm{Y}[2-0]$ and $\mathrm{Y}[2-0]$ | See Note A in Figure 8 |  | $15 \quad 30$ | ps |
| $t_{\text {Duty }}$ | Output duty-cycle distortion ${ }^{(1)}$ | Crossing point-to-crossing point distortion | -50 | 50 | ps |
| $\mathrm{t}_{\text {sk(pp) }}$ | Part-to-part skew | Any Y, see Note B in Eiqure 8 |  | 50 | ps |
| $\mathrm{C}_{0}$ | Output capacitance | $\mathrm{V}_{\mathrm{O}}=\mathrm{V}_{\mathrm{DD}}$ or GND |  | 1 | pF |
| LOAD | Expected output load |  |  | 50 | $\Omega$ |

(1) For an $800-\mathrm{MHz}$ signal, the 50 -ps error would result in a duty-cycle distortion of $\pm 4 \%$ when driven by an ideal clock input signal.

## LVPECL INPUT-TO-LVPECL OUTPUT PARAMETERS

|  | PARAMETER | TEST CONDITIONS | MIN | TYP | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LVPECL INPUT-TO-LVPECL OUTPUT PARAMETER |  |  |  |  |  |  |
| $\mathrm{t}_{\mathrm{pd}(\mathrm{lh})}$ | Propagation delay rising edge | VOX to VOX | 320 |  | 600 | ps |
| $\mathrm{t}_{\mathrm{pd}(\mathrm{h})}$ | Propagation delay falling edge | VOX to VOX | 320 |  | 600 | ps |
| $\mathrm{t}_{\text {sk(p) }}$ | LVPECL pulse skew | VOX to VOX, see Note C in Eig. ure 8 |  |  | 100 | ps |

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## LVCMOS OUTPUT PARAMETER, Y3

| PARAMETER |  | TEST CONDITIONS |  | MIN | TYP | MAX | UNIT <br> MHz |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{f}_{\text {clk }}$ | OUTPUT frequency, see Figure $5^{(1)}$. |  |  | 0 |  | 200 |  |
| $\mathrm{t}_{\text {skLVCMOS(0) }}$ | Output skew between the LVCMOS output Y3 and LVPECL outputs Y[2:0] | VOX to $\mathrm{V}_{\mathrm{DD}} / 2$, see Figure 8 |  | 1.3 | 1.6 | 2.1 | ns |
| $\mathrm{t}_{\text {sk(pp) }}$ | Part-to-part skew | Y3, see Note B in Eigure 8. |  |  | 300 |  | ps |
| $\mathrm{V}_{\mathrm{OH}}$ | High-level output voltage | $V_{D D}=$ min to max | $\mathrm{I}_{\mathrm{OH}}=-100 \mu \mathrm{~A}$ | $\mathrm{V}_{\mathrm{DD}}-0.1$ |  |  | V |
|  |  | $V_{D D}=3 V$ | $\mathrm{I}_{\mathrm{OH}}=-6 \mathrm{~mA}$ | 2.4 |  |  |  |
|  |  | $V_{D D}=3 \mathrm{~V}$ | $\mathrm{I}_{\mathrm{OH}}=-12 \mathrm{~mA}$ | 2 |  |  |  |
| $\mathrm{V}_{\text {OL }}$ | Low-level output voltage | $V_{D D}=$ min to max | $\mathrm{I}_{\mathrm{LL}}=100 \mu \mathrm{~A}$ |  |  | 0.1 | V |
|  |  | $V_{D D}=3 \mathrm{~V}$ | $\mathrm{I}_{\mathrm{OL}}=6 \mathrm{~mA}$ |  |  | 0.5 |  |
|  |  | $V_{D D}=3 \mathrm{~V}$ | $\mathrm{l}_{\mathrm{OL}}=12 \mathrm{~mA}$ |  |  | 0.8 |  |
| IOH | High-level output current | $V_{D D}=3.3 \mathrm{~V}$ | $\mathrm{V}_{\mathrm{O}}=1.65 \mathrm{~V}$ |  | -29 |  | mA |
| $\mathrm{l}_{\mathrm{OL}}$ | Low-level output current | $\mathrm{V}_{\mathrm{DD}}=3.3 \mathrm{~V}$ | $\mathrm{V}_{\mathrm{O}}=1.65 \mathrm{~V}$ |  | 37 |  | mA |
| $\mathrm{l}_{\mathrm{Oz}}$ | High-impedance-state output current | $\mathrm{V}_{\mathrm{DD}}=3.6 \mathrm{~V}$ | $\mathrm{V}_{\mathrm{O}}=\mathrm{V}_{\mathrm{DD}}$ or 0 V |  |  | $\pm 5$ | $\mu \mathrm{A}$ |
| $\mathrm{C}_{0}$ | Output capacitance | $\mathrm{V}_{\mathrm{DD}}=3.3 \mathrm{~V}$ |  | 2 |  |  | pF |
| $\mathrm{t}_{\text {Duty }}$ | Output duty cycle distortion ${ }^{(2)}$ | Measured at $\mathrm{V}_{\mathrm{DD}} / 2$ |  | -150 |  | 150 | ps |
| $\mathrm{t}_{\text {pd(l/ }}$ ) | Propagation delay rising edge from IN to Y3 | VOX to $\mathrm{V}_{\mathrm{DD}} / 2$ load, see Eigure-1d |  | 1.6 |  | 2.6 | ns |
| $\mathrm{t}_{\text {pd(hl) }}$ | Propagation delay falling edge from IN to Y3 | VOX to $\mathrm{V}_{\mathrm{DD}} / 2$ load, see Figure-10 |  | 1.6 |  | 2.6 | ns |
| $\mathrm{t}_{\mathrm{r}}$ | Output rise slew rate | $20 \%$ to $80 \%$ of swing, see Eigure 10 |  | 1.4 | 2.3 |  | V/ns |
| $\mathrm{t}_{\mathrm{f}}$ | Output fall slew rate | 80\% to $20 \%$ of swing, see Eigure 1d |  | 1.4 | 2.3 |  | V/ns |

(1) Operating the CDCM1804 LVCMOS output above the maximum frequency does not cause a malfunction to the device, but the Y3 output will not achieve enough signal swing to meet the output specification. Therefore, the CDCM1804 can be operated at higher frequencies, while the LVCMOS output Y3 becomes unusable.
(2) For a $200-\mathrm{MHz}$ signal, the 150 -ps error would result in a duty cycle distortion of $\pm 3 \%$ when driven by an ideal clock input signal.

## JITTER CHARACTERISTICS

|  | PARAMETER | TEST CONDITIONS | MIN | TYP | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| ${ }^{\text {jitterLVPECL }}$ | Additive phase jitter from input to LVPECL output Y[2:0], see Eigure_2. | 12 kHz to 20 MHz , $\mathrm{f}_{\text {out }}=250 \mathrm{MHz}$ to 800 MHz , divide-by-1 mode |  |  | 0.15 | ps rms |
|  |  | 50 kHz to 40 MHz , $\mathrm{f}_{\text {out }}=250 \mathrm{MHz}$ to 800 MHz , divide-by-1 mode |  |  | 0.25 |  |
| $\mathrm{t}_{\mathrm{jitter} L \text { Lemos }}$ | Additive phase jitter from input to LVCMOS output Y3, see Eigure_3 | $12 \mathrm{kHz} \text { to } 20 \mathrm{MHz}, \mathrm{f}_{\text {out }}=250 \mathrm{MHz},$ divide-by-1 mode |  |  | 0.25 | ps rms |
|  |  | 50 kHz to $40 \mathrm{MHz}, \mathrm{f}_{\text {out }}=250 \mathrm{MHz}$, divide-by-1 mode |  |  | 0.4 |  |

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Figure 2.

LVPECL OUTPUT SWING
VREQUENCY


G003
Figure 4.

ADDITIVE PHASE NOISE
FREQUENCY OFFSET FROM CARRIER - LVCMOS


Figure 3.

LVCMOS OUTPUT SWING
FREQUENCY


G004
Figure 5.

## SUPPLY CURRENT ELECTRICAL CHARACTERISTICS

over recommended operating free-air temperature range (unless otherwise noted)

| PARAMETER |  |  | TEST CONDITIONS | MIN | TYP | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{I}_{\mathrm{DD}}$ | Supply current | Full load | All outputs enabled and terminated with $50 \Omega$ to $\mathrm{V}_{\mathrm{DD}}-2 \mathrm{~V}$ on LVPECL outputs and 10 pF on LVCMOS output, $f=800 \mathrm{MHz}$ for LVPECL outputs and 200 MHz for LVCMOS, $\mathrm{V}_{\mathrm{DD}}=3.3 \mathrm{~V}$ |  | 160 |  | mA |
|  |  | No load | Outputs enabled, no output load, $f=800 \mathrm{MHz}$ for LVPECL outputs and 200 MHz for LVCMOS, $\mathrm{V}_{\mathrm{DD}}=3.6 \mathrm{~V}$ |  |  | 110 |  |
|  | Supply current saving per LVPECL output stage disabled, no load |  | $f=800 \mathrm{MHz}$ for LVPECL output, $\mathrm{V}_{\mathrm{DD}}=3.3 \mathrm{~V}$ |  | 10 |  | mA |
| $\mathrm{I}_{\mathrm{DDZ}}$ | Supply current, 3-state |  | All outputs in the high-impedance state by control logic, $f=0$ Hz , $\mathrm{V}_{\mathrm{DD}}=3.6 \mathrm{~V}$ |  |  | 0.5 | mA |



Figure 6.

## PACKAGE THERMAL RESISTANCE

| PARAMETER | TEST CONDITIONS | MIN | TYP |
| :--- | :--- | :---: | :---: |
| $R_{\theta J A-1}$ QFN-24 package thermal resistance ${ }^{(1)}$ | 4-layer JEDEC test board (JESD51-7), <br> airflow $=0$ ft/min | 106.6 | UNIT |
| QFN-24 package thermal resistance <br> with thermal vias in PCB ${ }^{(1)}$ | 4-layer JEDEC test board (JESD51-7) with four <br> thermal vias of 22-mil diameter each, <br> airflow $=0 \mathrm{ft} / \mathrm{min}$ | 55.4 | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |

(1) It is recommended to provide four thermal vias to connect the thermal pad of the package effectively with the PCB and ensure a good heat sink.

## Example:

Calculation of the junction-lead temperature with a 4-layer JEDEC test board using four thermal vias:
$\mathrm{T}_{\text {Chassis }}=85^{\circ} \mathrm{C}$ (temperature of the chassis)
$P_{\text {effective }}=I_{\max } \times \mathrm{V}_{\max }=110 \mathrm{~mA} \times 3.6 \mathrm{~V}=396 \mathrm{~mW}$ (maximum power consumption inside the package)
$\theta \mathrm{T}_{\text {Junction }}=\mathrm{R}_{\theta \mathrm{JA}-2} \times \mathrm{P}_{\text {effective }}=55.45^{\circ} \mathrm{C} / \mathrm{W} \times 396 \mathrm{~mW}=21.96^{\circ} \mathrm{C}$
$T_{\text {Junction }}=\theta \mathrm{T}_{\text {Junction }}+\mathrm{T}_{\text {Chassis }}=21.96^{\circ} \mathrm{C}+85^{\circ} \mathrm{C}=107^{\circ} \mathrm{C}$ (the maximum junction temperature of $\mathrm{T}_{\text {die-max }}=125^{\circ} \mathrm{C}$ is not violated)

## CONTROL INPUT CHARACTERISTICS

over recommended operating free-air temperature range

|  | PARAMETER | TEST CONDITIONS | MIN | TYP | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{t}_{\text {su }}$ | Setup time, S0, S1, S2, and EN terminals before clock IN |  | 25 |  |  | ns |
| $\mathrm{th}_{\mathrm{h}}$ | Hold time, S0, S1, S2, and EN terminals after clock IN |  | 0 |  |  | ns |
| $\mathrm{t}_{\text {(disable) }}$ | Time between latching the EN low transition and when all outputs are disabled (how much time is required until the outputs turn off) |  |  | 10 |  | ns |
| ${ }^{\text {(enable) }}$ | Time between latching the EN low-to-high transition and when outputs are enabled based on control settings (how much time passes before the outputs carry valid signals) |  |  | 1 |  | $\mu \mathrm{s}$ |
| Rpullup | Internal pullup resistor on S [2:0] and EN inputs |  | 42 | 60 | 78 | k $\Omega$ |
| $\mathrm{V}_{\mathrm{IH}(\mathrm{H})}$ | Three-level input high, S0, S1, S2, and EN terminals ${ }^{(1)}$ |  | $0.9 \mathrm{~V}_{\mathrm{DD}}$ |  |  | V |
| $\mathrm{V}_{\text {IM(M) }}$ | Three-level input MID, S0, S1, S2, and EN terminals |  | $0.3 \mathrm{~V}_{\mathrm{DD}}$ |  | $0.7 \mathrm{~V}_{\mathrm{DD}}$ | V |
| $\mathrm{V}_{\text {IL(L) }}$ | Three-level input low, S0, S1, S2, and EN terminals |  |  |  | $0.1 \mathrm{~V}_{\mathrm{DD}}$ | V |
| $\mathrm{I}_{\mathrm{IH}}$ | Input current, S0, S1, S2, and EN terminals | $V_{1}=V_{D D}$ |  |  | -5 | $\mu \mathrm{A}$ |
| $\mathrm{I}_{\text {IL }}$ |  | $\mathrm{V}_{1}=$ GND | 38 |  | 85 | $\mu \mathrm{A}$ |

(1) Leaving this terminal floating automatically pulls the logic level high to $V_{D D}$ through an internal pullup resistor of $60 \mathrm{k} \Omega$.

## BIAS VOLTAGE VBB

over recommended operating free-air temperature range

| PARAMETER | TEST CONDITIONS | MIN | TYP | MAX |
| :---: | :---: | ---: | ---: | ---: |
| UNIT |  |  |  |  |
| VBB | Output reference voltage | $\mathrm{V}_{\mathrm{DD}}=3 \mathrm{~V}-3.6 \mathrm{~V}, \mathrm{I}_{\mathrm{BB}}=-0.2 \mathrm{~mA}$ | $\mathrm{~V}_{\mathrm{DD}}-1.4$ | $\mathrm{~V}_{\mathrm{DD}}-1.2$ | V (



Figure 7.

## PARAMETER MEASUREMENT INFORMATION



NOTES: A. Output skew, $\mathrm{t}_{\mathrm{sk}(0)}$, is calculated as the greater of:

- The difference between the fastest and the slowest $t_{p d(L H) n}(n=0 \ldots 2)$
- The difference between the fastest and the slowest $t_{p d(H L) n}(n=0 \ldots 2)$
B. Part-to-part skew, $\mathrm{t}_{\mathrm{sk}(\mathrm{pp})}$, is calculated as the greater of:
- The difference between the fastest and the slowest $t_{p d(L H) n}(n=0 \ldots 2$ for LVPECL, $n=3$ for LVCMOS) across multiple devices - The difference between the fastest and the slowest $t_{p d(H L) n}(n=0 \ldots 2$ for LVPECL, $n=3$ for LVCMOS) across multiple devices
C. Pulse skew, $\mathrm{t}_{\mathrm{sk}(\mathrm{p})}$, is calculated as the magnitude of the absolute time difference between the high-to-low ( $\mathrm{t}_{\mathrm{pd}(\mathrm{HL}}$ ) and the low-to-high $\left(\mathrm{t}_{\mathrm{pd}(\mathrm{LH})}\right)$ propagation delays when a single switching input causes one or more outputs to switch, $\mathrm{t}_{\mathrm{sk}(\mathrm{p})}=\left|\mathrm{t}_{\mathrm{pd}(\mathrm{HL})}-\mathrm{t}_{\mathrm{pd}(\mathrm{LH})}\right|$. Pulse skew is sometimes referred to as pulse width distortion or duty cycle skew.

Figure 8. Waveforms for Calculation of $\mathrm{t}_{\mathbf{s k}(0)}$ and $\mathrm{t}_{\mathbf{s k}(\mathrm{pp})}$


Figure 9. LVPECL Differential Output Voltage and Rise/Fall Time

PARAMETER MEASUREMENT INFORMATION (continued)


Figure 10. LVCMOS Output Loading During Device Test

## PCB DESIGN FOR THERMAL FUNCTIONALITY

It is recommended to take special care of the PCB design for good thermal flow from the QFN-24 terminal package to the PCB.
Due to the three LVPECL outputs, the current consumption of the CDCM1804 is fixed.
JEDEC JESD51-7 specifies thermal conductivity for standard PCB boards.
Modeling the CDCM1804 with a standard 4-layer JEDEC board results in a $67.22^{\circ} \mathrm{C}$ maximum temperature with $\mathrm{R}_{\text {日JA }}$ of $106.62^{\circ} \mathrm{C} / \mathrm{W}$ for $25^{\circ} \mathrm{C}$ ambient temperature.
When deploying four thermal vias (one per quadrant), the thermal flow improves significantly, yielding $46.94^{\circ} \mathrm{C}$ maximum temperature with $\mathrm{R}_{\text {日JA }}$ of $55.4^{\circ} \mathrm{C} / \mathrm{W}$ for $25^{\circ} \mathrm{C}$ ambient temperature.

To ensure sufficient thermal flow, it is recommended to design with four thermal vias in applications enabling all four outputs at once.

## PARAMETER MEASUREMENT INFORMATION (continued)



M0029-01
Figure 11. Recommended Thermal Via Placement
See the application reports Quad Flatpack No-Lead Logic Packages (SCBA017) and QFN/SON PCB Attachment (SLUA271) for further package-related information.

INSTRUMENTS
www.ti.com

## APPLICATION INFORMATION

## LVPECL RECEIVER INPUT TERMINATION

The input of the CDCM1804 has a high impedance and comes with a large common-mode voltage range.
For optimized noise performance, it is recommended to properly terminate the PCB trace (transmission line). If a differential signal drives the CDCM1804, then a $100-\Omega$ termination resistor is recommended to be placed as close as possible across the input terminals. An even better approach is to install $2 \times 50 \Omega$, with the center tap connected to a capacitor (C) to terminate odd-mode noise and make up for transmission-line mismatches. The VBB output can also be connected to the center tap to bias the input signal to $\left(\mathrm{V}_{\mathrm{DD}}-1.3 \mathrm{~V}\right)$ (see Figure - 12) .


Figure 12. Recommended AC-Coupling LVPECL Receiver Input Termination


Figure 13. Recommended DC-Coupling LVPECL Receiver Input Termination
The CDCM1804 can also be driven by single-ended signals. Typically, the input signal becomes connected to one input, while the complementary input must be properly biased to the center voltage of the incoming input signal. For LVCMOS signals, this would be $\mathrm{V}_{\mathrm{CC}} / 2$, realized by a simple voltage divider (e.g., two $10-\mathrm{k} \Omega$ resistors). The best option (especially if the dc offset of the input signal might vary) is to ac-couple the input signal and then rebias the signal using the VBB reference output. See Eigure-14.

## APPLICATION INFORMATION (continued)



NOTE:
$\mathrm{C}_{\mathrm{AC}}$ - AC-coupling capacitor (e.g., 10 nF )
$\mathrm{C}_{\mathrm{CT}}$ - Capacitor keeps voltage at $\overline{\mathrm{N}}$ constant (e.g., 10 nF )
$R_{d c}$ - Load and correct duty cycle (e.g., $50 \Omega$ )
VBB - Bias voltage output
Figure 14. Typical Application Setting for Single-Ended Input Signals Driving the CDCM1804

## DEVICE BEHAVIOR DURING RESET AND CONTROL-TERMINAL SWITCHING

Output Behavior From Enabling the Device ( $\mathrm{EN}=0 \rightarrow 1$ )
In disable mode ( $\mathrm{EN}=0$ ), all output drivers are switched in high-Z mode. The $\mathrm{S}[2: 0]$ control inputs are also switched off. In the same mode, all flip-flops are reset. The typical current consumption is below $500 \mu \mathrm{~A}$.
When the device is enabled again, it takes typically $1 \mu \mathrm{~s}$ for the settling of the reference voltage and currents. During this time, the outputs $\mathrm{Y}[2: 0]$ and $\mathrm{Y}[2: 0]$ drive a high signal. Y 3 is unknown (could be high or low). After the settle time, the outputs go into the low state. Due to the synchronization of each output driver signal with the input clock, the state of the waveforms after enabling the device is as shown in Eigure 15. The inverting input and output signal are not included. The $\mathrm{Y}: / 1$ waveform is the undivided output driver state.

## APPLICATION INFORMATION (continued)



Figure 15. Waveforms

## Enabling a Single Output Stage

If a single output stage becomes enabled:

- $Y[2: 0]$ is either low or high (undefined).
- $\mathrm{Y}[2: 0]$ is the inverted signal of $\mathrm{Y}[2: 0]$.

With the first positive clock transition, the undivided output becomes the input clock state. The divided output states are equal to the actual internal divider. The internal divider is not reset while enabling single-output drivers.

## APPLICATION INFORMATION (continued)



T0069-01
Figure 16. Signal State After an Output Driver Becomes Enabled While $\operatorname{IN}=0$


Figure 17. Signal State After an Output Driver Becomes Enabled While IN = 1

## PACKAGING INFORMATION

| Orderable Device | Status <br> (1) | Package Type | Package Drawing | Pins | Package Qty | Eco Plan <br> (2) | Lead/Ball Finish <br> (6) | MSL Peak Temp <br> (3) | Op Temp ( ${ }^{\circ} \mathrm{C}$ ) | Device Marking (4/5) | Samples |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| CDCM1804RGER | ACTIVE | VQFN | RGE | 24 | 3000 | Green (RoHS \& no $\mathrm{Sb} / \mathrm{Br}$ ) | NIPDAU | Level-2-260C-1 YEAR | -40 to 85 | $\begin{aligned} & \text { CDCM } \\ & 1804 \end{aligned}$ | Samples |
| CDCM1804RGET | ACTIVE | VQFN | RGE | 24 | 250 | Green (RoHS \& no $\mathrm{Sb} / \mathrm{Br}$ ) | NIPDAU | Level-2-260C-1 YEAR | -40 to 85 | $\begin{aligned} & \text { CDCM } \\ & 1804 \end{aligned}$ | Samples |
| SN0305042RTHR | ACTIVE | VQFN | RGE | 24 | 3000 | Green (RoHS \& no $\mathrm{Sb} / \mathrm{Br}$ ) | NIPDAU | Level-2-260C-1 YEAR | -40 to 85 | $\begin{aligned} & \text { CDCM } \\ & 1804 \end{aligned}$ | Samples |
| SN0305042RTHT | ACTIVE | VQFN | RGE | 24 | 250 | Green (RoHS \& no Sb/Br) | NIPDAU | Level-2-260C-1 YEAR | -40 to 85 | $\begin{aligned} & \text { CDCM } \\ & 1804 \end{aligned}$ | Samples |

${ }^{(1)}$ The marketing status values are defined as follows:
ACTIVE: Product device recommended for new designs.
LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.
NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.
PREVIEW: Device has been announced but is not in production. Samples may or may not be available.
OBSOLETE: TI has discontinued the production of the device.
${ }^{(2)}$ RoHS: TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed $0.1 \%$ by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free".
RoHS Exempt: TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption
Green: TI defines "Green" to mean the content of Chlorine (CI) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.
${ }^{(3)}$ MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.
${ }^{(4)}$ There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.
${ }^{(5)}$ Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a " $\sim$ " will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.
${ }^{(6)}$ Lead/Ball Finish - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead/Ball Finish values may wrap to two lines if the finish value exceeds the maximum column width.

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## TAPE AND REEL INFORMATION



| Device | Package Type | Package Drawing | Pins | SPQ | Reel Diameter $(\mathrm{mm})$ | Reel <br> Width <br> W1 (mm) | $\begin{gathered} \mathrm{AO} \\ (\mathrm{~mm}) \end{gathered}$ | $\begin{gathered} \mathrm{BO} \\ (\mathrm{~mm}) \end{gathered}$ | $\begin{gathered} \text { K0 } \\ (\mathrm{mm}) \end{gathered}$ | $\begin{gathered} \text { P1 } \\ (\mathrm{mm}) \end{gathered}$ | $\begin{gathered} \mathrm{W} \\ (\mathrm{~mm}) \end{gathered}$ | Pin1 <br> Quadrant |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| CDCM1804RGER | VQFN | RGE | 24 | 3000 | 330.0 | 12.4 | 4.3 | 4.3 | 1.5 | 8.0 | 12.0 | Q2 |
| CDCM1804RGET | VQFN | RGE | 24 | 250 | 180.0 | 12.4 | 4.3 | 4.3 | 1.5 | 8.0 | 12.0 | Q2 |


*All dimensions are nominal

| Device | Package Type | Package Drawing | Pins | SPQ | Length (mm) | Width (mm) | Height (mm) |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| CDCM1804RGER | VQFN | RGE | 24 | 3000 | 350.0 | 350.0 | 43.0 |
| CDCM1804RGET | VQFN | RGE | 24 | 250 | 210.0 | 185.0 | 35.0 |



Images above are just a representation of the package family, actual package may vary. Refer to the product data sheet for package details.


## NOTES:

1. All linear dimensions are in millimeters. Any dimensions in parenthesis are for reference only. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. The package thermal pad must be soldered to the printed circuit board for thermal and mechanical performance.


NON SOLDER MASK

SOLDER MASK DETAILS

NOTES: (continued)
4. This package is designed to be soldered to a thermal pad on the board. For more information, see Texas Instruments literature number SLUA271 (www.ti.com/lit/slua271).
5. Solder mask tolerances between and around signal pads can vary based on board fabrication site.


SOLDER PASTE EXAMPLE
BASED ON 0.125 mm THICK STENCIL
EXPOSED PAD
80\% PRINTED COVERAGE BY AREA
SCALE: 20X

NOTES: (continued)
6. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.

RTH (S-PVQFN-N24) PLASTIC QUAD FLATPACK


NOTES:
A. All linear dimensions are in millimeters. Dimensioning and tolerancing per ASME Y14.5M-1994.
B. This drawing is subject to change without notice.
C. QFN (Quad Flatpack No-Lead) Package configuration.
(D) The package thermal pad must be soldered to the board for thermal and mechanical performance. See the Product Data Sheet for details regarding the exposed thermal pad dimensions.

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