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35µV

130dB

120dB

130dB

3MHz

4V/µs

930µA

30mV

35nV/√Hz



# LMV2011 High Precision, Rail-to-Rail Output Operational Amplifier

### **General Description**

The LMV2011 is a new precision amplifier that offers unprecedented accuracy and stability at an affordable price and is offered in miniature (SOT23-5) package and in 8 lead SOIC package. This device utilizes patented techniques to measure and continually correct the input offset error voltage. The result is an amplifier which is ultra stable over time and temperature. It has excellent CMRR and PSRR ratings, and does not exhibit the familiar 1/f voltage and current noise increase that plagues traditional amplifiers. The combination of the LMV2011 characteristics makes it a good choice for transducer amplifiers, high gain configurations, ADC buffer amplifiers, DAC I-V conversion, and any other 2.7V-5V application requiring precision and long term stability.

Other useful benefits of the LMV2011 are rail-to-rail output, a low supply current of  $930\mu A$ , and wide gain-bandwidth product of 3MHz. These extremely versatile features found in the LMV2011 provide high performance and ease of use.

### Features

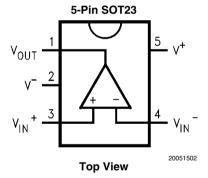
(For Vs = 5V, Typical unless otherwise noted)

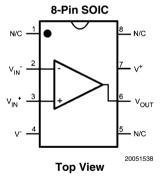
- Low Guaranteed V<sub>os</sub> over temperature
- Low Noise with no 1/f
- High CMRR
- High PSRRHigh Aug
- High A<sub>VOL</sub>
  Wide gain-bandwidth product
- High slew rate
- Low supply current
- Rail-to-rail output
- No external capacitors required

### **Applications**

- Precision Instrumentation Amplifiers
- Thermocouple Amplifiers
- Strain Gauge Bridge Amplifier

# Connection Diagrams





## **Ordering Information**

Package	Part Number	Package Marking	Transport Media	NSC Drawing	
	LMV2011MF	1k Units Tape and Reel		MF05A	
5-Pin SOT23 LMV2011MFX		A84A	3k Units Tape and Reel	I MIFUSA	
LMV2011MA		LMV2011MA	95 Units/Rail	MORA	
8-Pin SOIC	LMV2011MAX		2.5k Units Tape and Reel	- M08A	

## Absolute Maximum Ratings (Note 1)

If Military/Aerospace specified devices are required, please contact the National Semiconductor Sales Office/ Distributors for availability and specifications.

ESD Tolerance	
Human Body Model	2000V
Machine Model	200V
Supply Voltage	5.5V
Common-Mode Input Voltage	$-0.3 \le V_{CM} \le V_{CC} + 0.3V$
Differential Input Voltage	± Supply Voltage
Current At Input Pin	30mA

Current At Output Pin	30mA
Current At Power Supply Pin	50mA
Junction Temperature (T <sub>J</sub> )	150°C
Lead Temperature (soldering 10 sec.)	+300°C

## Operating Ratings (Note 1)

Supply Voltage	2.7V to 5.25V
Storage Temperature Range	–65°C to 150°C
Operating Temperature Range	0°C to 70°C

**2.7V DC Electrical Characteristics** Unless otherwise specified, all limits guaranteed for  $T_J = 25^{\circ}C$ ,  $V^+ = 2.7V$ ,  $V^- = 0V$ ,  $V_{CM} = 1.35V$ ,  $V_0 = 1.35V$  and  $R_L > 1M\Omega$ . Boldface limits apply at the temperature extremes.

Symbol	Parameter	Conditions	Min	Тур	Max	Units
V <sub>OS</sub>	Input Offset Voltage			0.8	25 <b>35</b>	μV
	Offset Calibration Time			0.5	10 <b>12</b>	ms
TCV <sub>OS</sub>	Input Offset Voltage			0.015		μV/°C
	Long-Term Offset Drift			0.006		µV/month
	Lifetime V <sub>OS</sub> Drift			2.5	5	μV
I <sub>IN</sub>	Input Current			-3		pА
l <sub>os</sub>	Input Offset Current			6		pА
R <sub>IND</sub>	Input Differential Resistance			9		MΩ
CMRR	Common Mode Rejection Ratio	$-0.3 \le V_{CM} \le 0.9V$ $0 \le V_{CM} \le 0.9V$		130	95 <b>90</b>	dB
PSRR	Power Supply Rejection Ratio	2.7V ≤ V+ ≤ 5V		120	95 <b>90</b>	dB
A <sub>VOL</sub> Open Loop Voltage Gain	Open Loop Voltage Gain	$R_L = 10k\Omega$		130	95 <b>90</b>	- dB
		$R_L = 2k\Omega$		124	90 <b>85</b>	UD
V <sub>O</sub> Output	Output Swing	$R_L = 10k\Omega$ to 1.35V V <sub>IN</sub> (diff) = ±0.5V	2.665 <b>2.655</b>	2.68		- v
				0.033	0.060 <b>0.075</b>	
		$R_L = 2k\Omega$ to 1.35V V <sub>IN</sub> (diff) = ±0.5V	2.630 <b>2.615</b>	2.65		- v
				0.061	0.085 <b>0.105</b>	v
Ι <sub>ο</sub>	Output Current	Sourcing, $V_O = 0V$ $V_{IN}(diff) = \pm 0.5V$		12	5 <b>3</b>	
		Sinking, V <sub>O</sub> = 5V V <sub>IN</sub> (diff) = ±0.5V		18	5 <b>3</b>	- mA
R <sub>OUT</sub>	Output Impedance			0.05		Ω
I <sub>s</sub>	Supply Current			0.919	1.20 <b>1.50</b>	mA

$V_{\rm O} = 1.35$ V, and R <sub>L</sub> >	

Symbol	Parameter	Conditions	6	Min	Тур	Max	Units
GBW	Gain-Bandwidth Product				3		MHz
SR	Slew Rate				4		V/µs
θ <sub>m</sub>	Phase Margin				60		Deg
G <sub>m</sub>	Gain Margin				-14		dB
e <sub>n</sub>	Input-Referred Voltage Noise				35		nV/√Hz
i <sub>n</sub>	Input-Referred Current Noise				150		fA/√Hz
e <sub>n</sub> p-p	Input-Referred Voltage Noise	$R_s = 100\Omega$ , DC to 10Hz			850		nV <sub>pp</sub>
t <sub>rec</sub>	Input Overload Recovery Time				50		ms
t <sub>s</sub>	Output Settling Time	$A_V = -1, R_L = 2k\Omega$	1%		0.9		μs
		1V Step	0.1%		49		
			0.01%		100		1

# **5V DC Electrical Characteristics** Unless otherwise specified, all limits guaranteed for T<sub>J</sub> = 25°C, V<sup>+</sup> = 5V, V<sup>-</sup> = 0V, V<sub>CM</sub> = 2.5V, V<sub>0</sub> = 2.5V and R<sub>L</sub> > 1MΩ. Boldface limits apply at the temperature extremes.

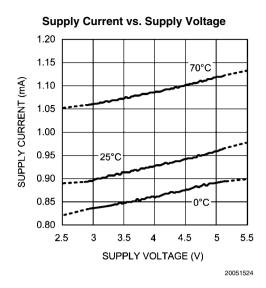
Symbol	Parameter	Conditions	Min	Тур	Мах	Units
V <sub>OS</sub>	Input Offset Voltage			0.12	25 <b>35</b>	μV
	Offset Calibration Time			0.5	10 <b>12</b>	ms
TCV <sub>OS</sub>	Input Offset Voltage			0.015		μV/°C
	Long-Term Offset Drift			0.006		µV/month
	Lifetime V <sub>OS</sub> Drift			2.5	5	μV
IN	Input Current			-3		рА
os	Input Offset Current			6		рА
R <sub>IND</sub>	Input Differential Resistance			9		MΩ
CMRR	Common Mode Rejection Ratio	$-0.3 \le V_{CM} \le 3.2$ $0 \le V_{CM} \le 3.2$		130	100 <b>90</b>	dB
PSRR	Power Supply Rejection Ratio	$2.7V \le V^+ \le 5V$		120	95 <b>90</b>	dB
A <sub>VOL</sub> Open Loop Voltage Gai	Open Loop Voltage Gain	$R_L = 10k\Omega$		130	105 <b>100</b>	- dB
		$R_L = 2k\Omega$		132	95 <b>90</b>	
V <sub>O</sub> Output Swir	Output Swing	$R_L = 10k\Omega$ to 2.5V V <sub>IN</sub> (diff) = ±0.5V	4.96 <b>4.95</b>	4.978		
				0.040	0.070 <b>0.085</b>	
		$R_L = 2k\Omega$ to 2.5V V <sub>IN</sub> (diff) = ±0.5V	4.895 <b>4.875</b>	4.919		- v
				0.091	0.115 <b>0.140</b>	
I <sub>O</sub>	Output Current	Sourcing, V <sub>O</sub> = 0V V <sub>IN</sub> (diff) = ±0.5V		15	8 <b>6</b>	A
		Sinking, $V_0 = 5V$ V <sub>IN</sub> (diff) = ±0.5V		17	8 <b>6</b>	- mA
R <sub>OUT</sub>	Output Impedance			0.05		Ω
s	Supply Current per Channel			0.930	1.20 <b>1.50</b>	mA

# **5V AC Electrical Characteristics** $T_J = 25^{\circ}C$ , $V^+ = 5V$ , $V^- = 0V$ , $V_{CM} = 2.5V$ , $V_O = 2.5V$ , and $R_L > 1M\Omega$ . **Boldface** limits apply at the temperature extremes.

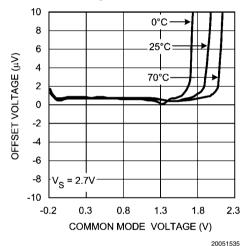
Symbol	Parameter	Conditions	6	Min	Тур	Max	Units
GBW	Gain-Bandwidth Product				3		MHz
SR	Slew Rate				4		V/µs
θ <sub>m</sub>	Phase Margin				60		deg
G <sub>m</sub>	Gain Margin				-15		dB
e <sub>n</sub>	Input-Referred Voltage Noise				35		nV/√Hz
i <sub>n</sub>	Input-Referred Current Noise				150		fA/√Hz
e <sub>n</sub> p-p	Input-Referred Voltage Noise	R <sub>S</sub> = 100Ω, DC to 10Hz			850		nV <sub>pp</sub>
t <sub>rec</sub>	Input Overload Recovery Time				50		ms
t <sub>s</sub>	Output Settling Time	$A_V = -1, R_L = 2k\Omega$	1%		0.8		us
		1V Step	0.1%		36		
			0.01%		100		

Note 1: Absolute Maximum Ratings indicate limits beyond which damage may occur. Operating Ratings indicate conditions for which the device is intended to be functional, but specific performance is not guaranteed. For guaranteed specifications and test conditions, see the Electrical Characteristics.

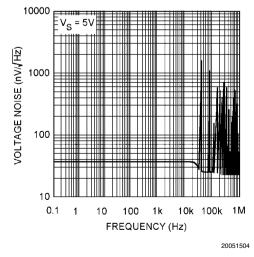
# **Typical Performance Characteristics** $T_A=25C$ , $V_S=5V$ unless otherwise specified.

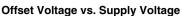


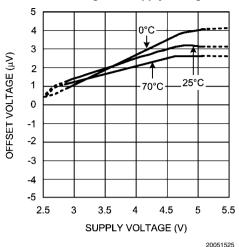
Offset Voltage vs. Common Mode



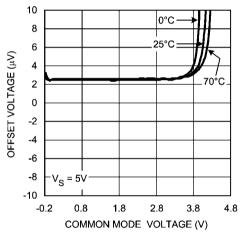
Voltage Noise vs. Frequency





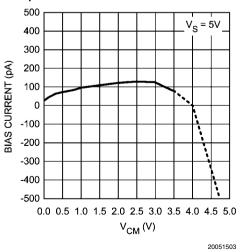


Offset Voltage vs. Common Mode

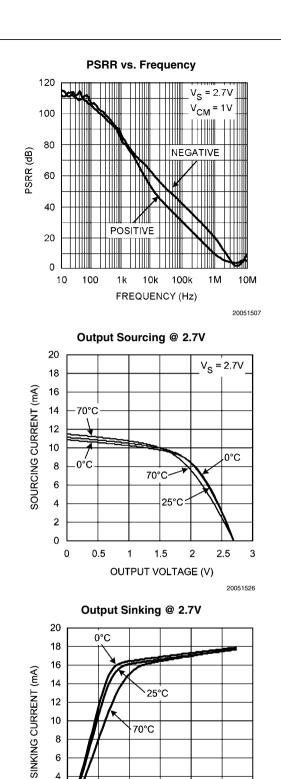


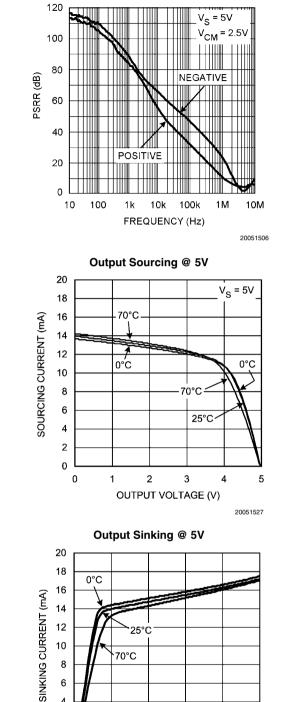
20051534

Input Bias Current vs. Common Mode









V<sub>S</sub> = 5V

**PSRR vs. Frequency** 

0.5

1.5

OUTPUT VOLTAGE (V)

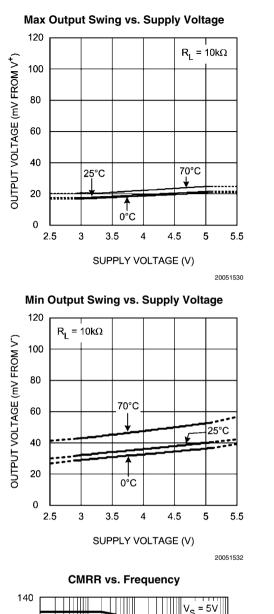


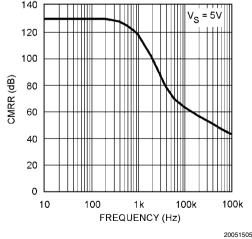
V<sub>S</sub> = 2.7V

2.5

OUTPUT VOLTAGE (V)







120  $R_1 = 2k\Omega$ OUTPUT VOLTAGE (mV FROM V<sup>+</sup>) 100 25°C 70°C 80 60 0°C 40 20 0 2.5 3 3.5 4.5 5 5.5 4 SUPPLY VOLTAGE (V) 20051531 Min Output Swing vs. Supply Voltage 120 70°C OUTPUT VOLTAGE (mV FROM V') 100 25°C 80 60 0°C 40 20  $R_L = 2k\Omega$ 0 2.5 3 3.5 4 4.5 5.5 5 SUPPLY VOLTAGE (V) 20051533 Open Loop Gain and Phase vs. Supply Voltage 100 150.0 ٧s = 5\ 80 120.0 PHASE = 5V 60 90.0 GAIN (dB) PHASE ( 60.0 40 GAIN 20 30.0 R, = 1M 0.0 0 < 20pF С 's vs = 2.7V OR 5V

Max Output Swing vs. Supply Voltage

20051508

-30.0

10M

-20

100

1k

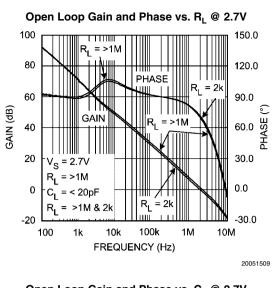
10k

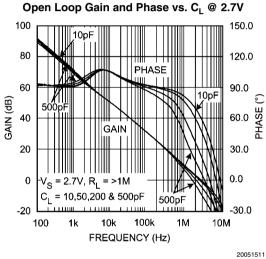
100k

FREQUENCY (Hz)

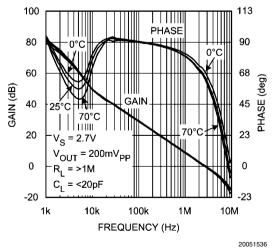
1M

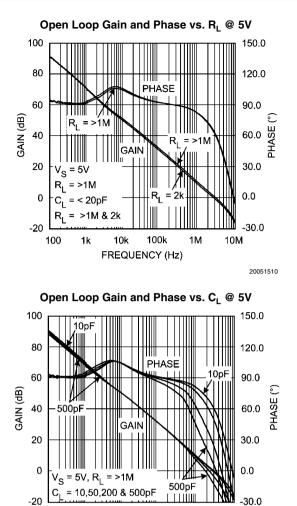






Open Loop Gain and Phase vs. Temperature @ 2.7V





20051512

10M

Open Loop Gain and Phase vs. Temperature @ 5V

FREQUENCY (Hz)

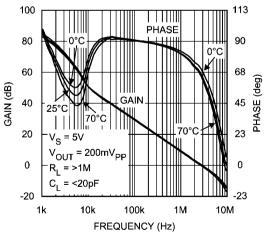
100k

1M

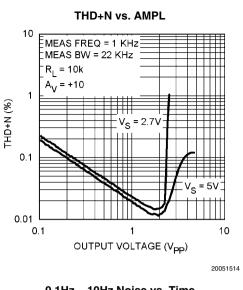
100

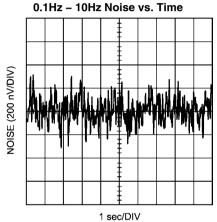
1k

10k

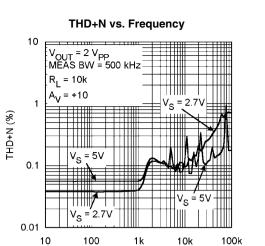


20051537





20051515



FREQUENCY (Hz)

20051513

LMV2011

#### Application Information THE BENEFITS OF LMV2011 NO 1/f NOISE

Using patented methods, the LMV2011 eliminates the 1/f noise present in other amplifiers. That noise, which increases as frequency decreases, is a major source of measurement error in all DC-coupled measurements. Low-frequency noise appears as a constantly-changing signal in series with any measurement being made. As a result, even when the measurement is made rapidly, this constantly-changing noise signal will corrupt the result. The value of this noise signal can be surprisingly large. For example: If a conventional amplifier has a flat-band noise level of  $10nV/\sqrt{Hz}$  and a noise corner of 10Hz, the RMS noise at 0.001Hz is  $1\mu V//Hz$ . This is equivalent to a 0.50µV peak-to-peak error, in the frequency range 0.001 Hz to 1.0 Hz. In a circuit with a gain of 1000, this produces a 0.50mV peak-to-peak output error. This number of 0.001 Hz might appear unreasonably low, but when a data acquisition system is operating for 17 minutes, it has been on long enough to include this error. In this same time, the LMV2011 will only have a 0.21mV output error. This is smaller by 2.4 x. Keep in mind that this 1/f error gets even larger at lower frequencies. At the extreme, many people try to reduce this error by integrating or taking several samples of the same signal. This is also doomed to failure because the 1/f nature of this noise means that taking longer samples just moves the measurement into lower frequencies where the noise level is even higher.

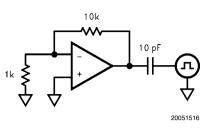
The LMV2011 eliminates this source of error. The noise level is constant with frequency so that reducing the bandwidth reduces the errors caused by noise.

Another source of error that is rarely mentioned is the error voltage caused by the inadvertent thermocouples created when the common "Kovar type" IC package lead materials are soldered to a copper printed circuit board. These steel-based leadframe materials can produce over  $35\mu V/^{\circ}C$  when soldered onto a copper trace. This can result in thermocouple noise that is equal to the LMV2011 noise when there is a temperature difference of only 0.0014°C between the lead and the board!

For this reason, the lead-frame of the LMV2011 is made of copper. This results in equal and opposite junctions which cancel this effect. The extremely small size of the SOT-23 package results in the leads being very close together. This further reduces the probability of temperature differences and hence decreases thermal noise.

#### **OVERLOAD RECOVERY**

The LMV2011 recovers from input overload much faster than most chopper-stabilized opamps. Recovery from driving the amplifier to 2X the full scale output, only requires about 40ms. Many chopper-stabilized amplifiers will take from 250ms to several seconds to recover from this same overload. This is because large capacitors are used to store the unadjusted offset voltage.



**FIGURE 1. Overload Recovery Test** 

The wide bandwidth of the LMV2011 enhances performance when it is used as an amplifier to drive loads that inject transients back into the output. ADCs (Analog-to-Digital Converters) and multiplexers are examples of this type of load. To simulate this type of load, a pulse generator producing a 1V peak square wave was connected to the output through a 10pF capacitor. (Figure 1) The typical time for the output to recover to 1% of the applied pulse is 80ns. To recover to 0.1% requires 860ns. This rapid recovery is due to the wide bandwidth of the output stage and large total GBW.

#### NO EXTERNAL CAPACITORS REQUIRED

The LMV2011 does not need external capacitors. This eliminates the problems caused by capacitor leakage and dielectric absorption, which can cause delays of several seconds from turn-on until the amplifier's error has settled.

#### MORE BENEFITS

The LMV2011 offers the benefits mentioned above and more. It has a rail-to-rail output and consumes only  $950\mu$ A of supply current while providing excellent DC and AC electrical performance. In DC performance, the LMC2001 achieves 130dB of CMRR, 120dB of PSRR and 130dB of open loop gain. In AC performance, the LMV2011 provides 3MHz of gain-bandwidth product and  $4V/\mu$ s of slew rate.

#### HOW THE LMV2011 WORKS

The LMV2011 uses new, patented techniques to achieve the high DC accuracy traditionally associated with chopper-stabilized amplifiers without the major drawbacks produced by chopping. The LMV2011 continuously monitors the input offset and corrects this error. The conventional chopping process produces many mixing products, both sums and differences, between the chopping frequency and the incoming signal frequency. This mixing causes large amounts of distortion, particularly when the signal frequency approaches the chopping frequency. Even without an incoming signal, the chopper harmonics mix with each other to produce even more trash. If this sounds unlikely or difficult to understand, look at the plot (Figure 2), of the output of a typical (MAX432) chopper-stabilized opamp. This is the output when there is no incoming signal, just the amplifier in a gain of -10 with the input grounded. The chopper is operating at about 150Hz; the rest is mixing products. Add an input signal and the noise gets much worse. Compare this plot with Figure 3 of the LMV2011. This data was taken under the exact same conditions. The auto-zero action is visible at about 30kHz but note the absence of mixing products at other frequencies. As a result, the LMV2011 has very low distortion of 0.02% and very low mixing products.

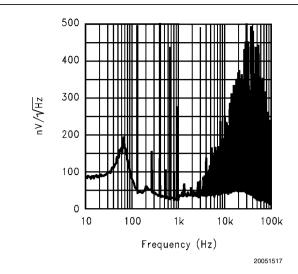


FIGURE 2. The Output of a Chopper Stabilized Op Amp (MAX432)

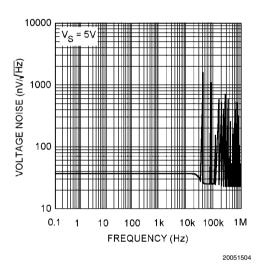


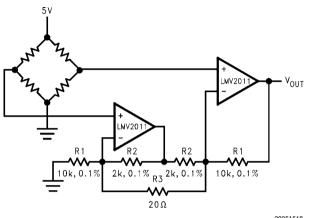
FIGURE 3. The Output of the LMV2011

#### INPUT CURRENTS

The LMV2011's input currents are different than standard bipolar or CMOS input currents in that it appears as a current flowing in one input and out the other. Under most operating conditions, these currents are in the picoamp level and will have little or no effect in most circuits. These currents tend to increase slightly when the common-mode voltage is near the minus supply. (See the typical curves.) At high temperatures such as 85°C, the input currents become larger, 0.5nA typical, and are both positive except when the V<sub>CM</sub> is near V<sup>-</sup>. If operation is expected at low common-mode voltages and high temperature, do not add resistance in series with the inputs to balance the impedances. Doing this can cause an increase in offset voltage. A small resistance such as 1k $\Omega$  can provide some protection against very large transients or overloads, and will not increase the offset significantly.

#### PRECISION STRAIN-GAUGE AMPLIFIER

This Strain-Gauge amplifier (Figure 4) provides high gain (1006 or ~60 dB) with very low offset and drift. Using the resistors' tolerances as shown, the worst case CMRR will be greater than 108 dB. The CMRR is directly related to the resistor mismatch. The rejection of common-mode error, at the output, is independent of the differential gain, which is set by R3. The CMRR is further improved, if the resistor ratio matching is improved, by specifying tighter-tolerance resistors, or by trimming.



20051518

FIGURE 4. Precision Strain Gauge Amplifier

# Extending Supply Voltages and Output Swing by Using a Composite Amplifier Configuration:

In cases where substantially higher output swing is required with higher supply voltages, arrangements like the ones shown in Figure 5 and Figure 6 could be used. These configurations utilize the excellent DC performance of the LMV2011 while at the same time allow the superior voltage and frequency capabilities of the LM6171 to set the dynamic performance of the overall amplifier. For example, it is possible to achieve ±12V output swing with 300MHz of overall GBW  $(A_v = 100)$  while keeping the worst case output shift due to V<sub>OS</sub> less than 4mV. The LMV2011 output voltage is kept at about mid-point of its overall supply voltage, and its input common mode voltage range allows the V- terminal to be grounded in one case (Figure 5, inverting operation) and tied to a small non-critical negative bias in another (Figure 6, noninverting operation). Higher closed-loop gains are also possible with a corresponding reduction in realizable bandwidth. Table 1 shows some other closed loop gain possibilities along with the measured performance in each case.

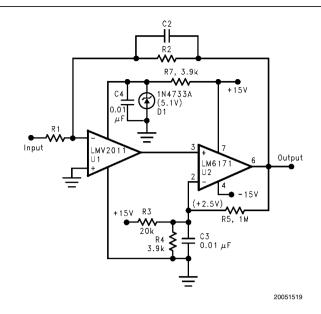


FIGURE 5. Composite Amplifier Configuration

A <sub>V</sub>	R1	R2	C2	BW	SR	en p-p
	(Ω)	(Ω)	(pF)	(MHz)	(V/µs)	(mV <sub>PP</sub> )
50	200	10k	8	3.3	178	37
100	100	10k	10	2.5	174	70
100	1k	100k	0.67	3.1	170	70
500	200	100k	1.75	1.4	96	250
1000	100	100k	2.2	0.98	64	400

**TABLE 1. Composite Amplifier Measured Performance** 

In terms of the measured output peak-to-peak noise, the following relationship holds between output noise voltage,  $e_n p_p$ , for different closed-loop gain,  $A_V$ , settings, where -3dB Bandwidth is BW:

$$\frac{e_{npp1}}{e_{npp2}} = \sqrt{\frac{BW1}{BW2}} \cdot \frac{A_V 1}{A_V 2}$$
(1)

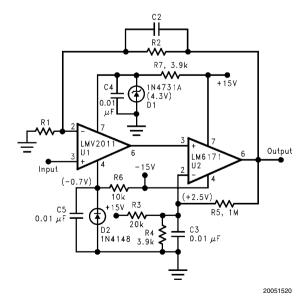


FIGURE 6. Composite Amplifier Configuration

It should be kept in mind that in order to minimize the output noise voltage for a given closed-loop gain setting, one could minimize the overall bandwidth. As can be seen from Equation 1 above, the output noise has a square-root relationship to the Bandwidth.

In the case of the inverting configuration, it is also possible to increase the input impedance of the overall amplifier, by raising the value of R1, without having to increase the feed-back resistor, R2, to impractical values, by utilizing a "Tee" network as feedback. See the LMC6442 data sheet (Application Notes section) for more details on this.

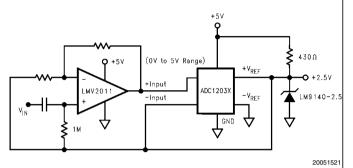


FIGURE 7. AC Coupled ADC Driver

#### LMV2011 AS ADC INPUT AMPLIFIER

The LMV2011 is a great choice for an amplifier stage immediately before the input of an ADC (Analog-to-Digital Converter), whether AC or DC coupled. See Figure 7 and Figure 8. This is because of the following important characteristics:

- A) Very low offset voltage and offset voltage drift over time and temperature allow a high closed-loop gain setting without introducing any short-term or long-term errors. For example, when set to a closed-loop gain of 100 as the analog input amplifier for a 12-bit A/D converter, the overall conversion error over full operation temperature and 30 years life of the part (operating at 50°C) would be less than 5 LSBs.
- B) Fast large-signal settling time to 0.01% of final value (1.4µs) allows 12 bit accuracy at 100KH<sub>Z</sub> or more sampling rate.
- **C)** No flicker (1/f) noise means unsurpassed data accuracy over any measurement period of time, no matter how long. Consider the following opamp performance, based on a typical low-noise, high-performance commercially-available device, for comparison:

Opamp flatband noise = 8nV/√Hz

1/f corner frequency = 100Hz

$$A_{V} = 2000$$

Measurement time = 100 sec

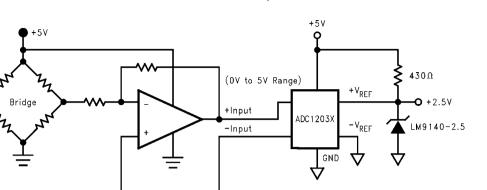
Bandwidth = 2Hz

This example will result in about 2.2 mV<sub>PP</sub> (1.9 LSB) of output noise contribution due to the opamp alone, compared to about  $594\mu V_{PP}$  (less than 0.5 LSB) when that opamp is replaced with the LMV2011 which has no 1/f contribution. If the measurement time is increased from 100 seconds to 1 hour, the improvement realized by using the LMV2011 would be a factor of about 4.8 times (2.86mV<sub>PP</sub> compared to 596 $\mu$ V when LMV2011 is used) mainly because the LMV2011 accuracy is not compromised by increasing the observation time.

D) Copper leadframe construction minimizes any thermocouple effects which would degrade low level/high gain data conversion application accuracy (see discussion under "The Benefits of the LMV2011" section above).

E) Rail-to-Rail output swing maximizes the ADC dynamic range in 5-Volt single-supply converter applications. Below are some typical block diagrams showing the LMV2011 used as an ADC amplifier (*Figure 7* and *Figure 8*).

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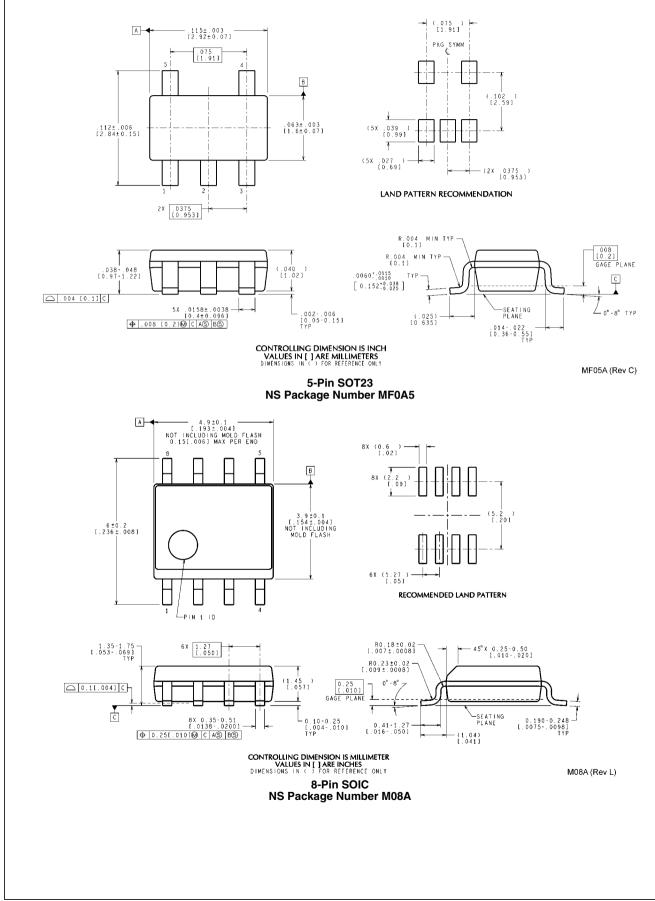


#### FIGURE 8. DC Coupled ADC Driver

LMV2011

## Physical Dimensions inches (millimeters) unless otherwise noted

LMV2011



# Notes

LMV2011

# Notes

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Displays	www.national.com/displays	Green Compliance	www.national.com/quality/green
Ethernet	www.national.com/ethernet	Packaging	www.national.com/packaging
Interface	www.national.com/interface	Quality and Reliability	www.national.com/quality
LVDS	www.national.com/lvds	Reference Designs	www.national.com/refdesigns
Power Management	www.national.com/power	Feedback	www.national.com/feedback
Switching Regulators	www.national.com/switchers		
LDOs	www.national.com/ldo		
LED Lighting	www.national.com/led		
PowerWise	www.national.com/powerwise		
Serial Digital Interface (SDI)	www.national.com/sdi		
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